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FINAL REPORT 250 kV ELECTRON GUN

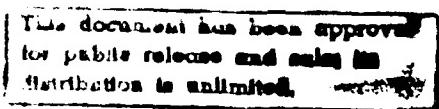
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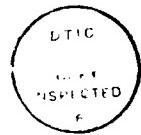
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Two high-voltage, high-power Pierce-type electron guns were designed and developed for use at the NRL high-power ubitron laboratory. The design of the high-voltage and vacuum housings of the guns incorporates design features utilized in the SLAC XK-5 klystron gun. Detail design data and beam trajectories are presented. Beam analyzer and high voltage tests are discussed. Assembly and detail drawings are included.		

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1.0 INTRODUCTION

1.1 PURPOSE

The purpose of this program was to develop a high-voltage, high-power Pierce-type electron gun to be used for experiments at the NRL high-power ubitron laboratory. These experiments are intended for high-power, high-quality electron-beam generation, beam diagnostics, and high-power microwave generation techniques.

1.2 SCOPE

In accordance with Contract No. N00014-85-C-2059 two electron guns were fabricated, pretested and delivered to NRL. The high-voltage and vacuum housings of the guns were consistent with the design utilized in the Stanford Linear Accelerator Center (SLAC) XK-5 klystron gun. This 12-month development program covers the period from December 1984 through December 1985.

The report describes details of beam optics calculations, performance characteristics, pretest results, and includes assembly and detail drawings along with a material list.

2.0 CALCULATIONS AND COMPUTED RESULTS

2.1 DIODE CHARACTERISTICS AND ELECTRON TRAJECTORIES

The process of arriving at optimum electron beam trajectories involves an iterative computational procedure and computer graphics plotting. Repetitive testing in the Varian computer controlled beam analyzer, to confirm the desired results, is limited to lower voltages (20 kV to 25 kV). Finalized electrostatic beam trajectories are illustrated in Figure 1 and Figure 2 for 20 kV and 250 kV respectively.

2.2 MAGNETIC FIELD

In the case of a confined-flow focusing system the magnetic field at the cathode can be determined approximately from the following expression:

$$B_c = \frac{(B_o) (\alpha)}{(r_c / r_o)^2} \text{ gauss}$$

where: B_c = Magnetic Field at Cathode

B_o = Main Field

r_c = Radius of Cathode

r_o = Radius of Beam

α = Cathode Flux Parameter

The mathematical expression for calculating is as follows:

$$\alpha = \sqrt{1 - \left(\frac{B_{br}}{B_o} \right)^2}$$

(6KM) --BUN FOR NPL. ELECTROSTATIC.
ITERATION 8

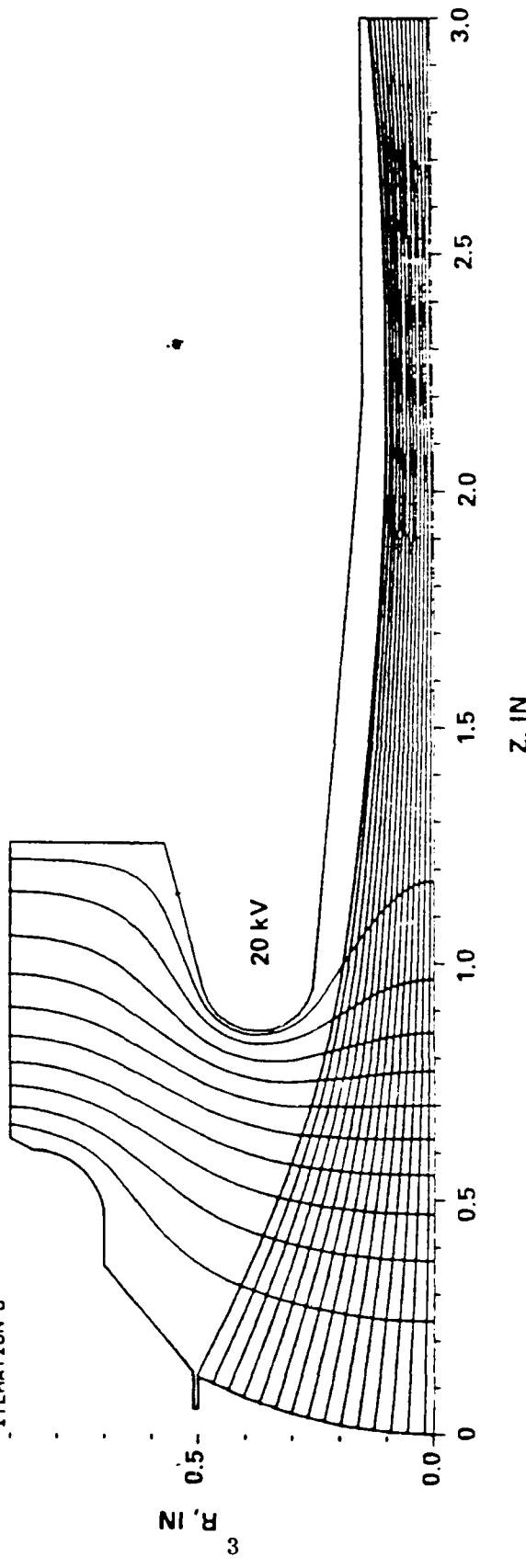


FIGURE 1. NONRELATIVISTIC BEAM TRAJECTORIES (20 KV)

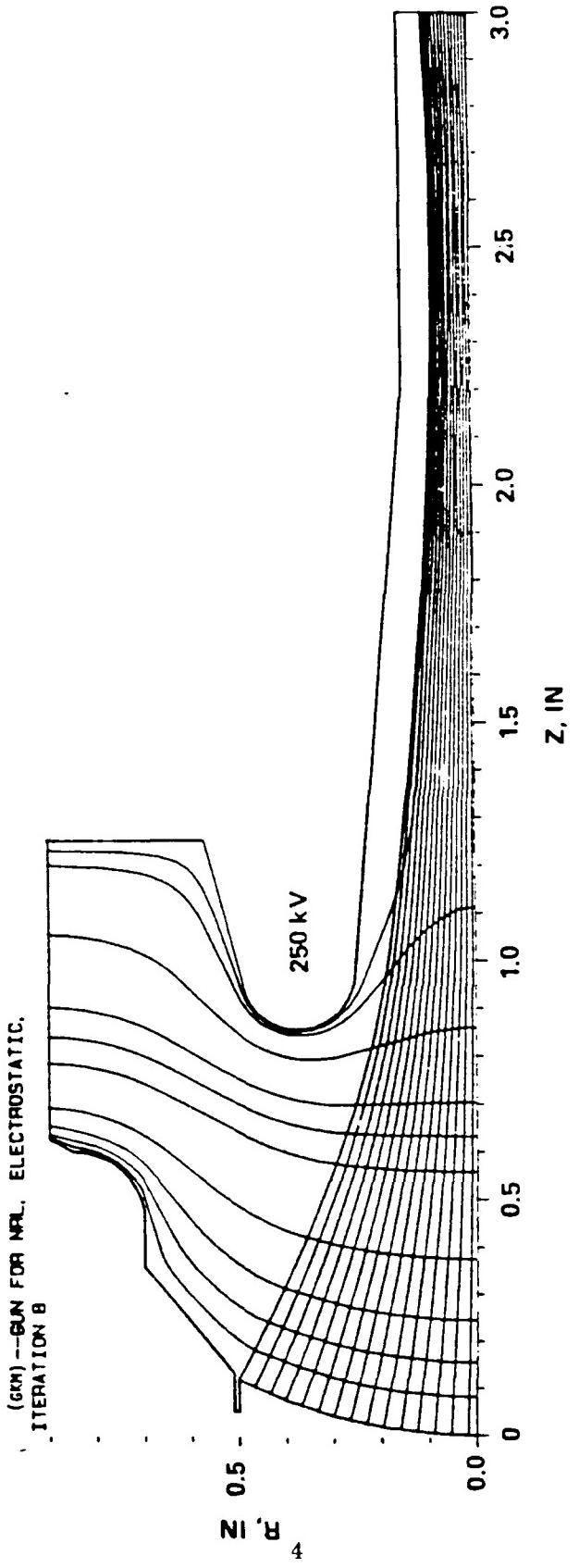


FIGURE 2. RELATIVISTIC BEAM TRAJECTORIES (250 kV)

where: B_{br} is the Brillouin field value and is equal to

$$B_{br} = \frac{463.5 \text{ (V) (k)}}{d} \quad (\text{For Low Beam Voltages})$$
$$= \left(\frac{468}{d} \right) \cdot \frac{\mu^{1/2}}{\left[\frac{\left(1 + \frac{V_o}{2 \times 510.98} \right)^{1/2}}{\frac{V_o}{510.98}} \right]^{1/2}} \quad \text{Relativistically Corrected } B_{BR}$$

Field

where: μ = Microperveance

V_o = Beam Voltage in kV

where: d = Beam Diameter (inches)

V = Beam Voltage

k = Perveance

The design magnetic field is calculated from these expressions and is plotted in Figure 3. (Relativistic)

2.3 COMPUTER GUN OPTICS DESIGN

With the aid of the Varian computer gun design programs, several designs were generated and analyzed. The gun electrode geometries were optimized in order to achieve the desired beam characteristics and voltage gradients around the focus electrode anode areas. Aside from determining the required perveance, convergence and voltage gradients, special attention was given to produce an extremely laminar beam in order to obtain the minimum axial velocity spread. In the final design, the velocity spread was computed to be 0.295%. Details of computer calculations were described in detail in previous reports.

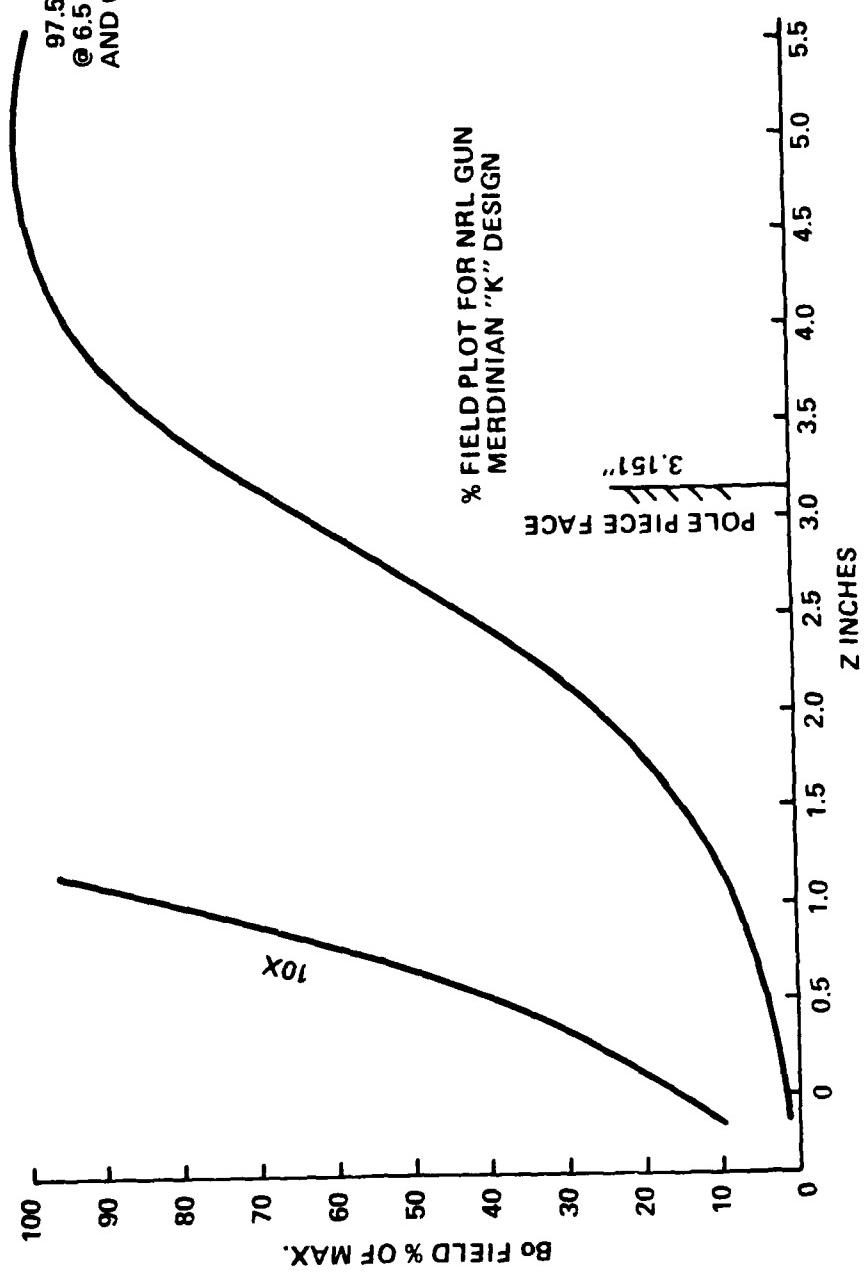


FIGURE 3. % MAGNETIC FIELD vs DISTANCE FROM CATHODE

In order to test the gun in the beam analyzer the tests can only be made at maximum voltage of 20 kV. The magnetic field was correspondingly adjusted.

3.0 DESIGN METHODOLOGY

The design and development of this electron gun followed a procedure which defines a certain sequence of events as described below:

1. A detailed computer analysis of the Pierce-type diode gun was performed at two beam voltages of 20 kV and 250 kV.
2. The beam trajectories in a confined-flow magnetic focusing field were calculated and plotted by the computer for 20 kV and 250 kV as illustrated in Figure 4 and Figure 5 respectively.
3. In order to ensure the integrity of the design at high-voltage operation, a computer plot of the voltage gradient in vacuum was generated as shown in Figure 6.
4. The electrostatic beam optics were then evaluated in a computer-controlled beam analyzer and the configuration refined for optimum performance.
5. Subsequently, the electron gun was placed in a confined-flow magnetic focusing field and retested. Reiterative modifications to the magnetic focusing field were introduced until satisfactory results were obtained.

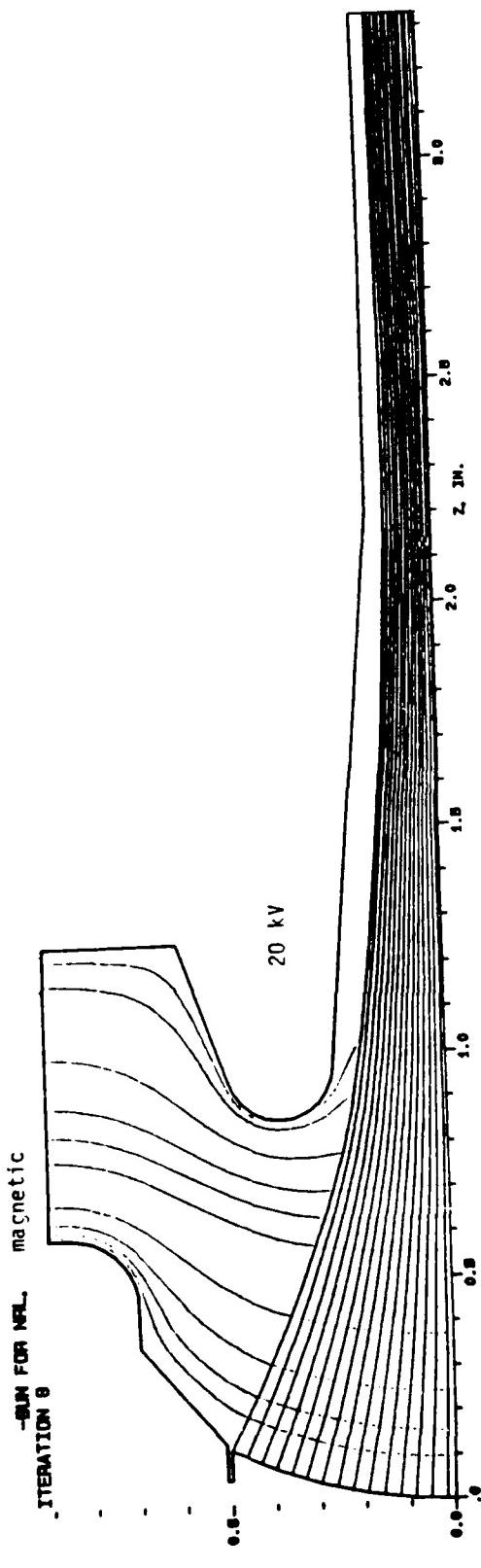


FIGURE 4. BEAM TRAJECTORIES IN CONFINED-FLOW MAGNETIC FOCUSING FIELD (20 kV)

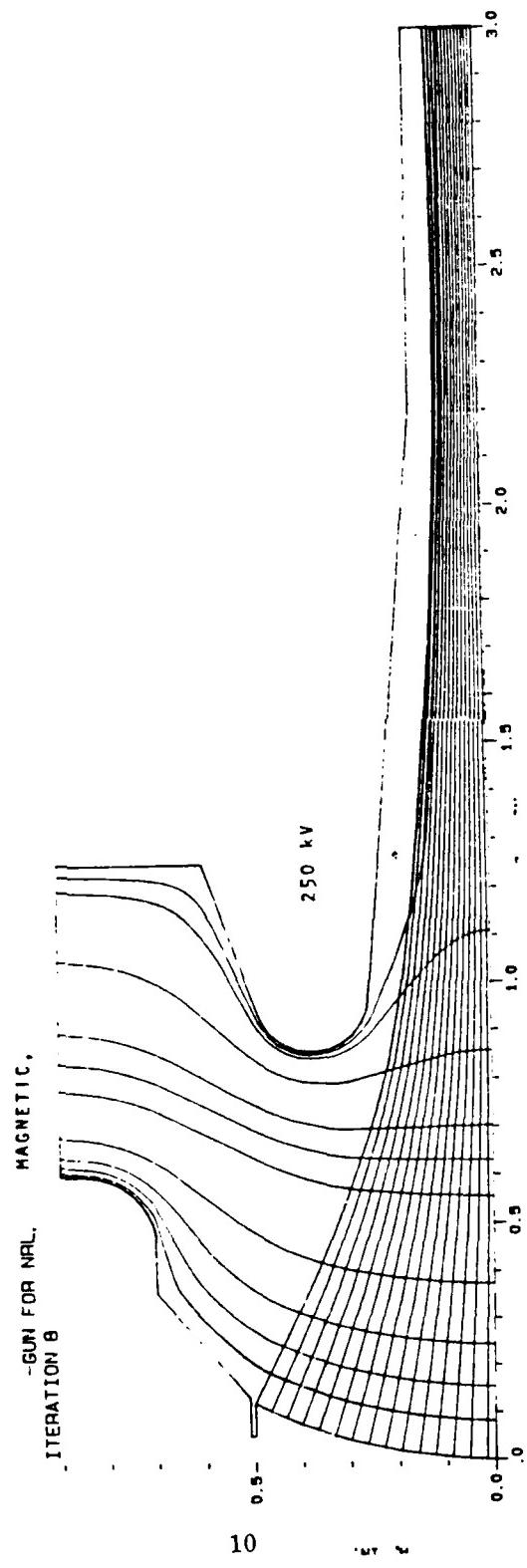


FIGURE 5. BEAM TRAJECTORIES IN CONFINED FLOW MAGNETIC FOCUSING FIELD (250 kV)

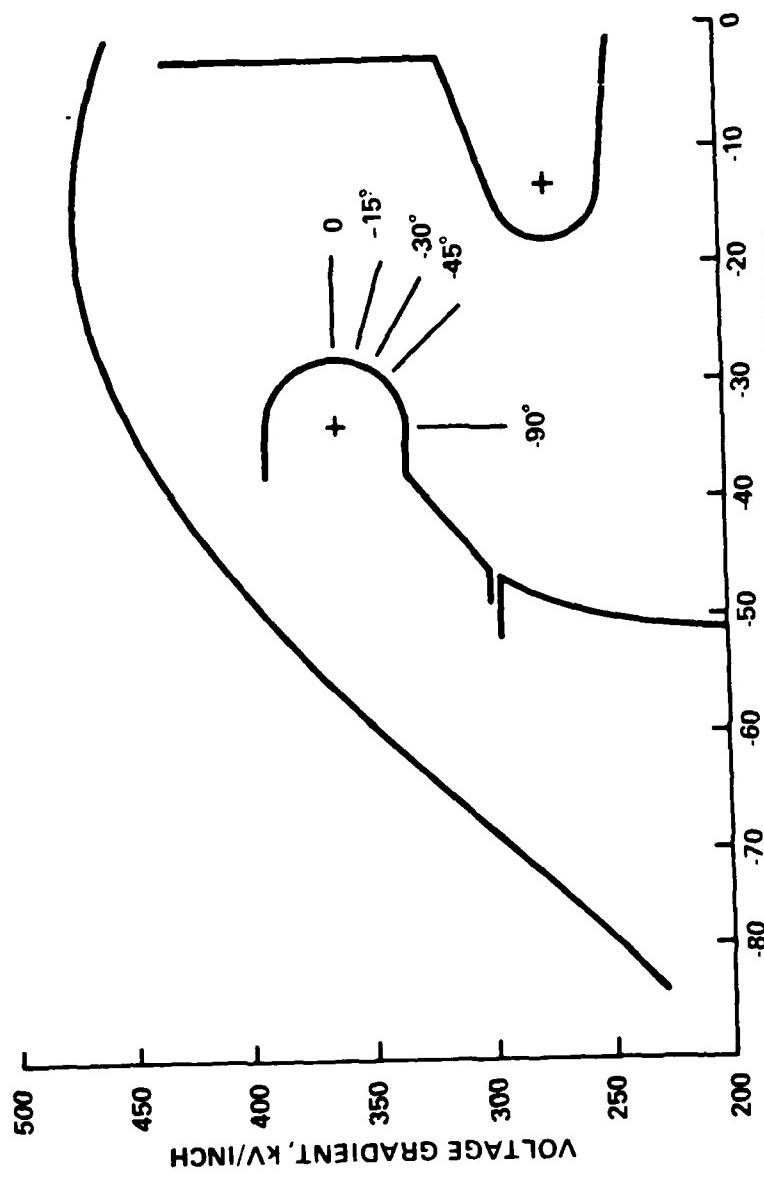


FIGURE 6. VOLTAGE GRADIENT vs FOCUS ELECTRON ANGLE

4.0 ELECTRON GUN SPECIFICATIONS

The finalized electron gun specifications as per Revision A dated 13 December 1984 are summarized below:

4.1	Operating Voltage (cathode pulse)	250 kV
4.2	Cathode Current	100 Amps
4.3	Cathode Heater Voltage (Nom.) (AC)	8.5 Volts
4.4	Cathode Heater Current (Nom.)	18.5 Amps
4.5	Pulse Length (Max)	2 μ sec
4.6	Repetition Rate (Max)	100 Hz
4.7	Beam Radius (in 2.5 kG Magnetic Field)	< 0.4 cm
4.8	Beam Centroid Offset (in 2.5 kG magnetic field)	<0.005 cm
4.9	Beam Axial Velocity Spread (biased standard deviation)	<0.4 % with a goal to 0.1% (= 8.5% beam ripple)
4.10	Beam Ripple (measured)	<20%
4.11	Concentricity of Cathode and Anode	<u>±0.004</u> inch
4.12	Angular Deviation (tilt) of Cathode and Anode Relative to Gun Axis (Max)	0.005 radius
4.13	Lifetime (Min)	5000 hrs
4.14	Capacitance (Max)	150 pF
4.15	Gun Connection to Tube (exit drift tube dia to be determined)	2-1/8" dia. Conflat® Flange
4.16	Gun Housing Dimensions	<SLAC XK-5 dimensions

5.0 ASSEMBLY DRAWINGS AND MATERIAL LIST

The electron gun is constructed from three major subassemblies as illustrated in Figure 7.

- High-Voltage Seal (Drawing Items 1 and 3)
- Cathode Assembly (Drawing Item 2)
- Iron Housing and Anode Assembly (Drawing Items 5 and 6)

The high-voltage seal and vacuum housing configuration is consistent with the design utilized in the SLAC XK-5 klystron gun. Assembly and detail drawings of the gun with a parts and material list are given in Appendix A. Cathode assembly is centered in the high-voltage seal assembly within 0.001 in all directions and secured to the base. (Heliarc area at point -3.626 and its associated dimensions are used for centering.)

Iron housing and anode assembly centering also related to the same -3.626 point with its own associated dimensions.

Finally, the iron housing is heliarced to the high-voltage seal assembly.

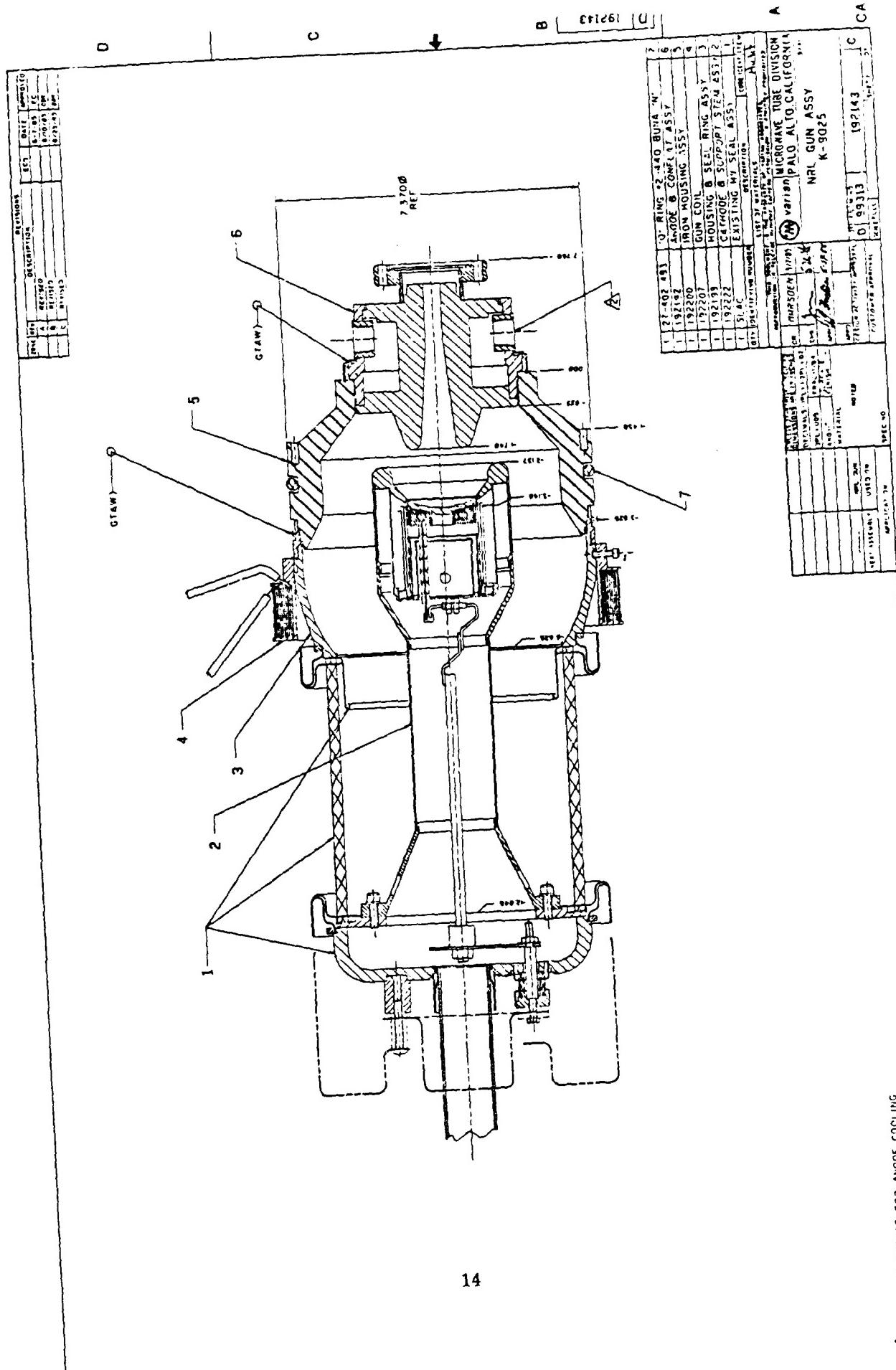


FIGURE 7. ELECTRON GUN ASSEMBLY DRAWING (R. JONES).

6.0 TEST RESULTS

6.1 HIGH-VOLTAGE HOLD-OFF TESTS

High-voltage tests were conducted on gun S/N 101. A negative dc voltage was applied to the cathode and gradually raised to 150 kV dc. This level of voltage was held for 10 minutes without arcing and is considered safe for low duty 300 kV two microsecond pulses. See reference in Appendix B titled "Electron Gun Breakdown" by Armand Staprans, Varian Associates, Inc., presented at the 1985 High-Voltage Workshop, February 26, 1985, Monterey, California.

6.2 BEAM ANALYZER TESTS

The first electron gun was tested in the Varian computer-controlled beam analyzer at non-relativistic voltages. The beam tester configuration used in these tests is illustrated in Figure 8. An electrostatic beam profile is shown in Figure 9. The beam diameter, perveance and beam minimum position closely corresponded to the computer predictions.

Magnetic beam analyzer tests have produced an excellent beam with the required perveance and beam diameter. The confined flow beam profiles for the gun are shown in Figure 10. To analyze the quality of the beam optics and magnetic match, the magnetic field was varied from 70 to 110% of the prescribed value with no change in the beam diameter or scalloping. Scalloping was measured to be below 3% in all cases.

A gun coil was used to trim the magnetic field threading the cathode. Varying the field in the gun coil affected the beam diameter with no significant effect on the scalloping. A three-dimensional beam shape in a confined-flow focused magnetic field is illustrated in Figure 11.

6.3 HIGH-VOLTAGE TEST

A short drift tube and isolated collector were fabricated and attached to the gun by means of a 2-3/4 inch Varian Conflat flange. The gun-body-

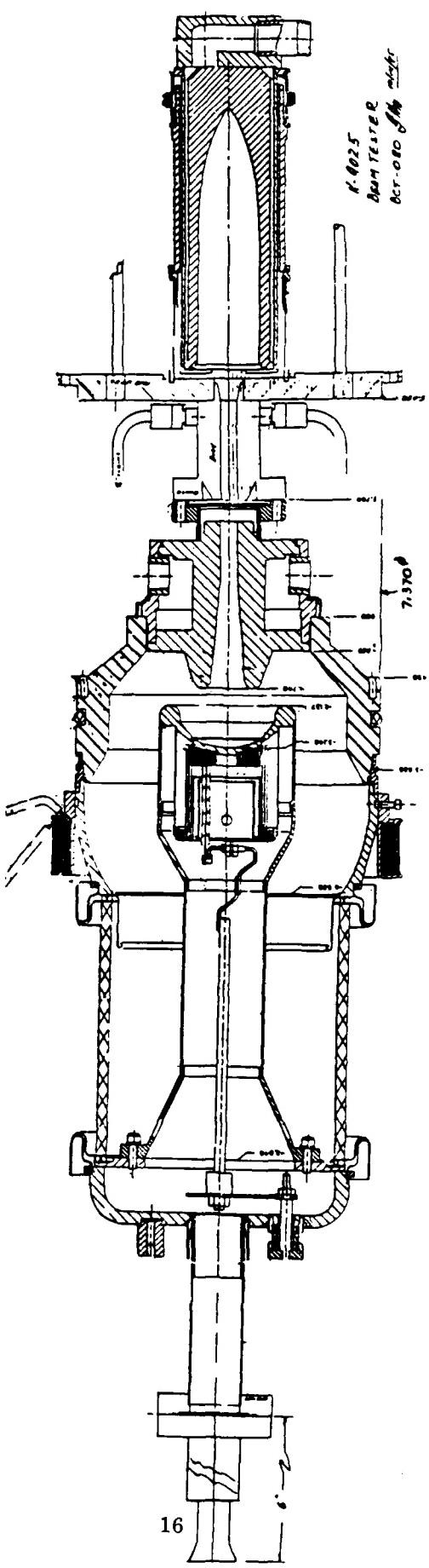


FIGURE 8. BEAM TESTER WITH K-9025 GUN

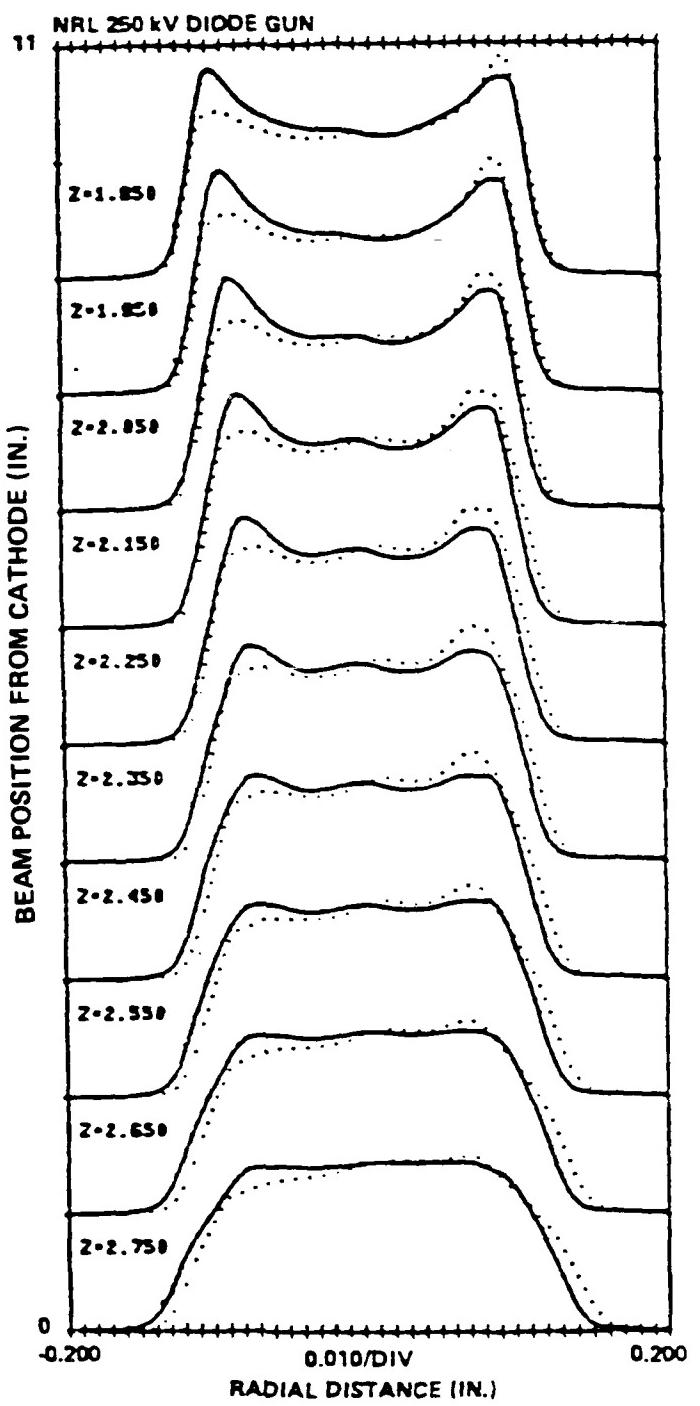


FIGURE 9. ELECTROSTATIC BEAM PROFILES

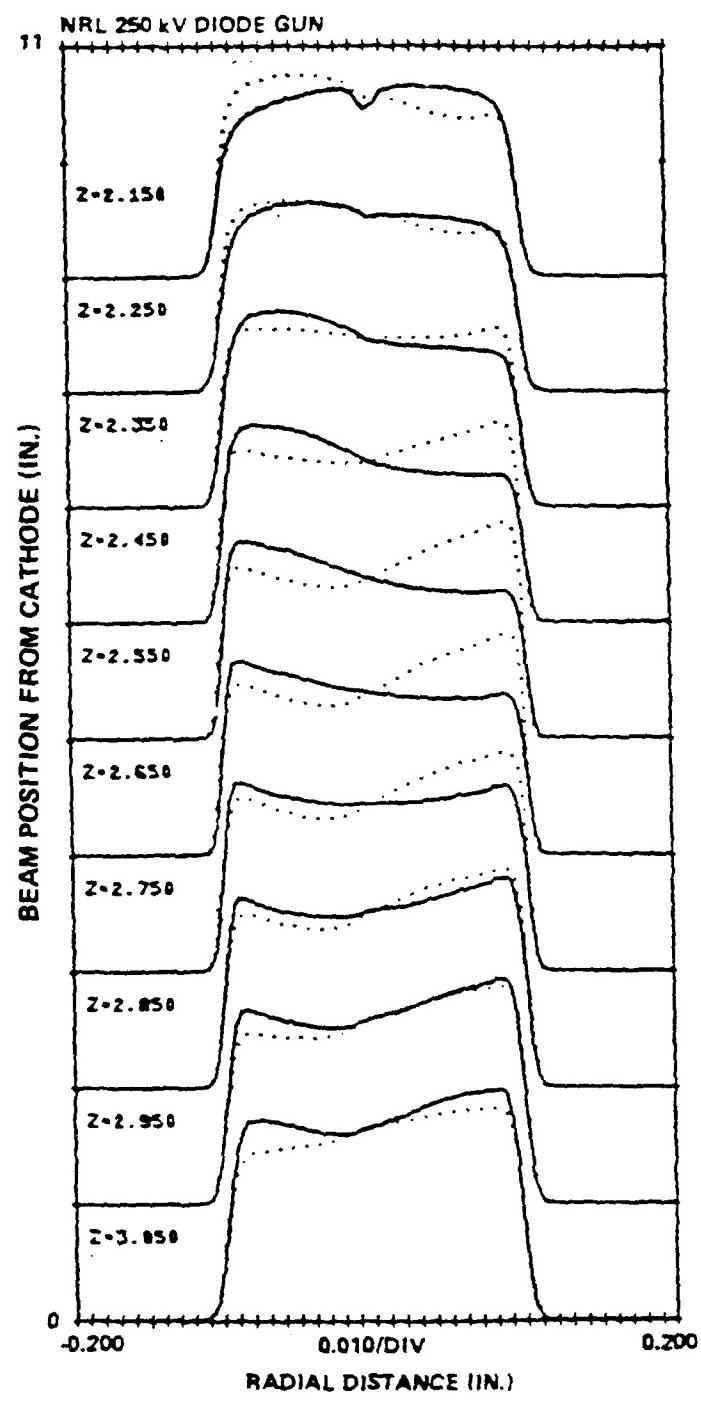


FIGURE 10. CONFINED-FLOW BEAM PROFILES

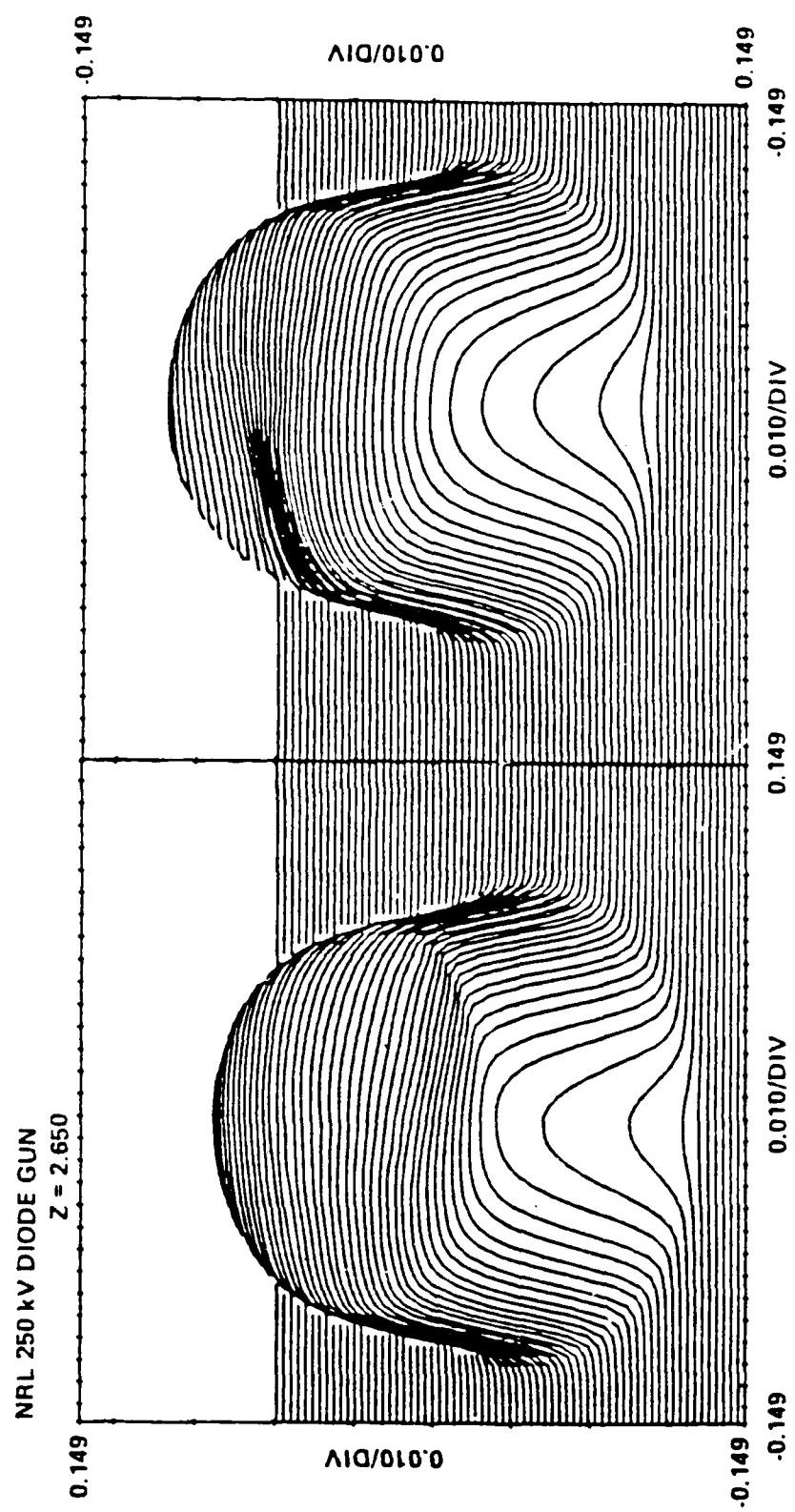


FIGURE 11. 3-D CURRENT DENSITY PROFILES

collector assembly was exhausted, baked out at 450°^oC, pinched off and tested under oil up to 150 kV dc.

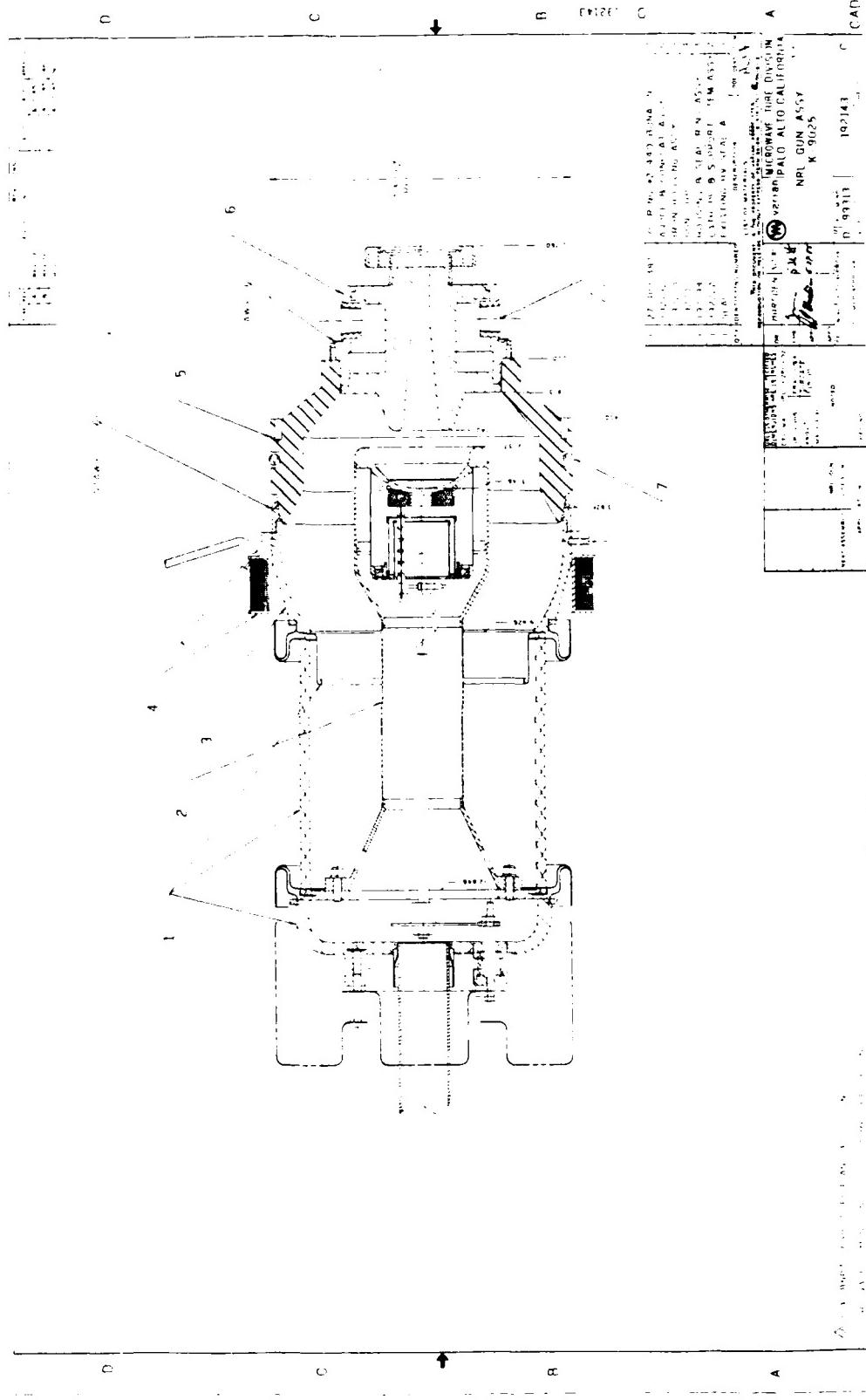
6.4 CONCLUSION

A high-quality, high-voltage gun with excellent beam laminarity has been developed for fast-wave device applications. The beam tester has been fabricated and is ready for test and evaluation. This high-power evaluation will be evaluated at NRL.

APPENDIX A

1. ELECTRON GUN ASSEMBLY DRAWING
2. DETAIL PARTS DRAWINGS
(Varian Associates, Inc.)
3. DETAIL PARTS DRAWINGS
(SLAC)
4. PARTS AND MATERIALS LIST

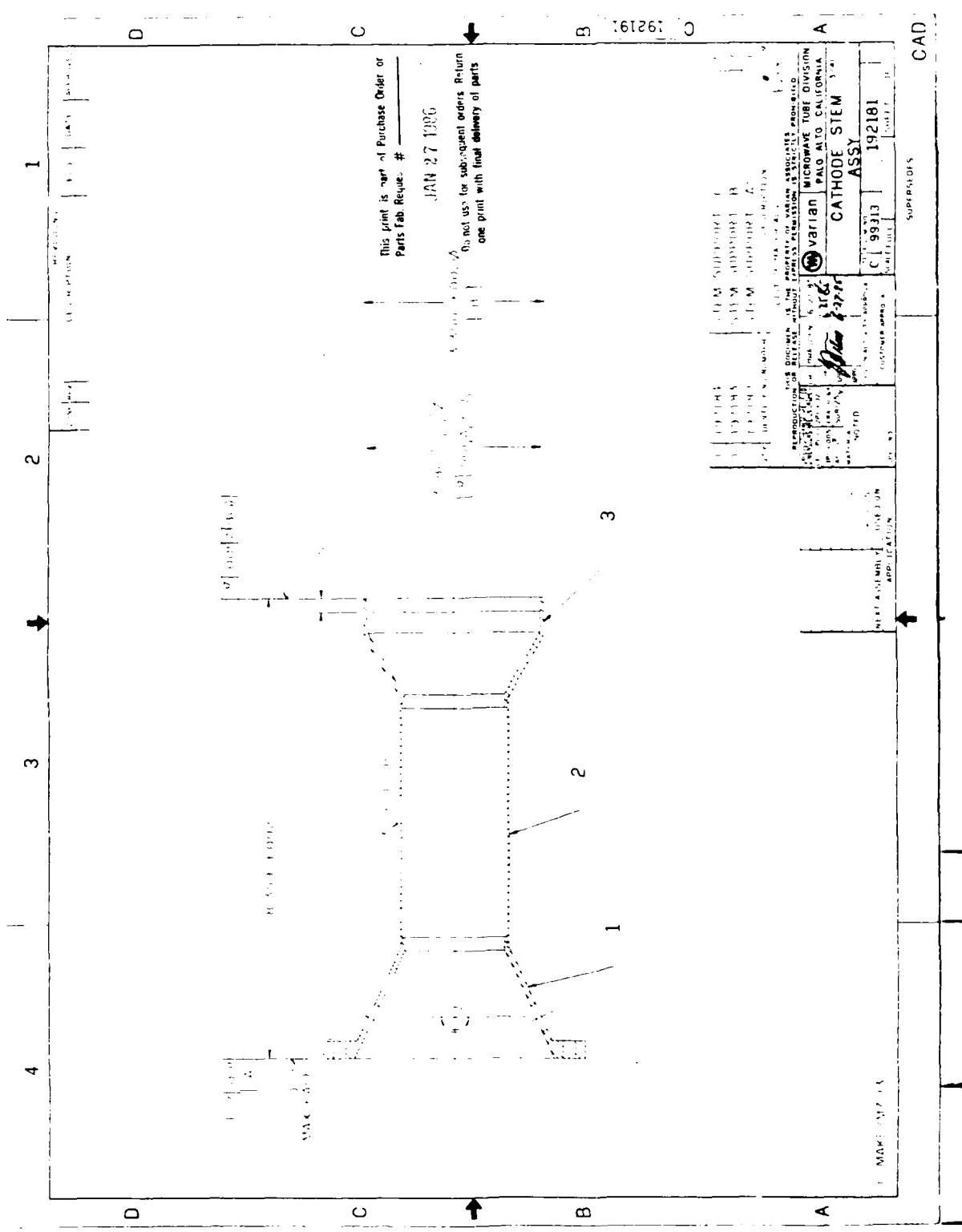
APPENDIX A-1
ELECTRON GUN ASSEMBLY DRAWING



A1

APPENDIX A-2

DETAIL PARTS DRAWINGS
(Varian Associates, Inc.)



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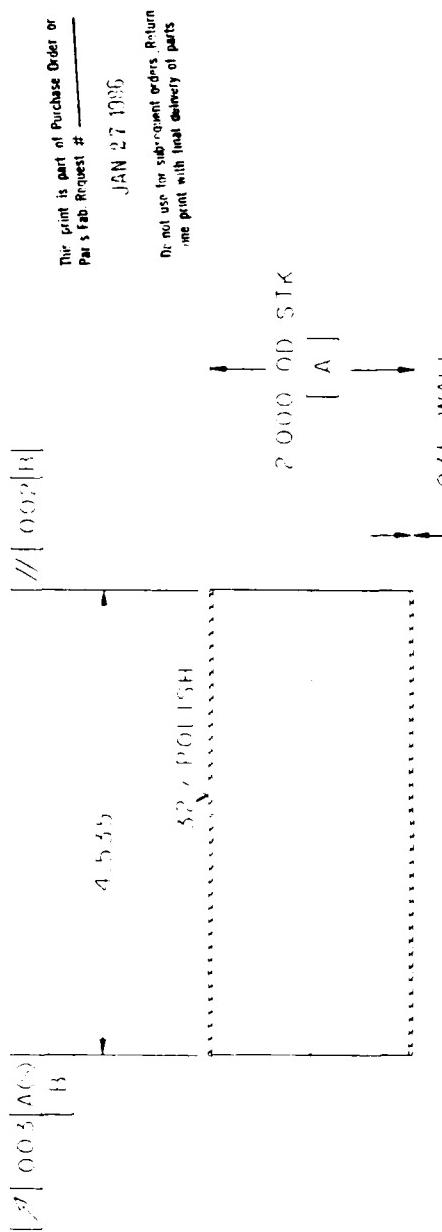
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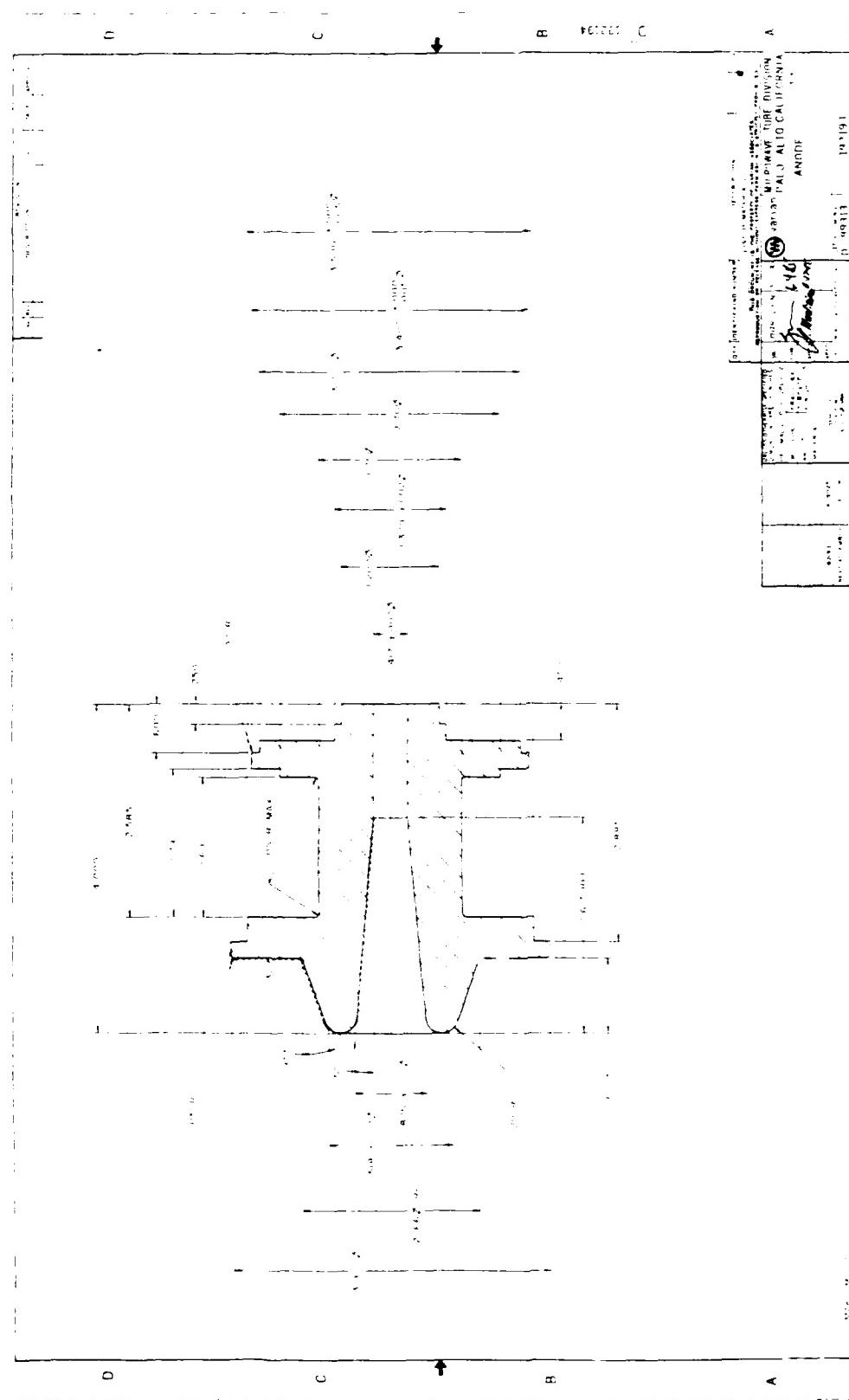
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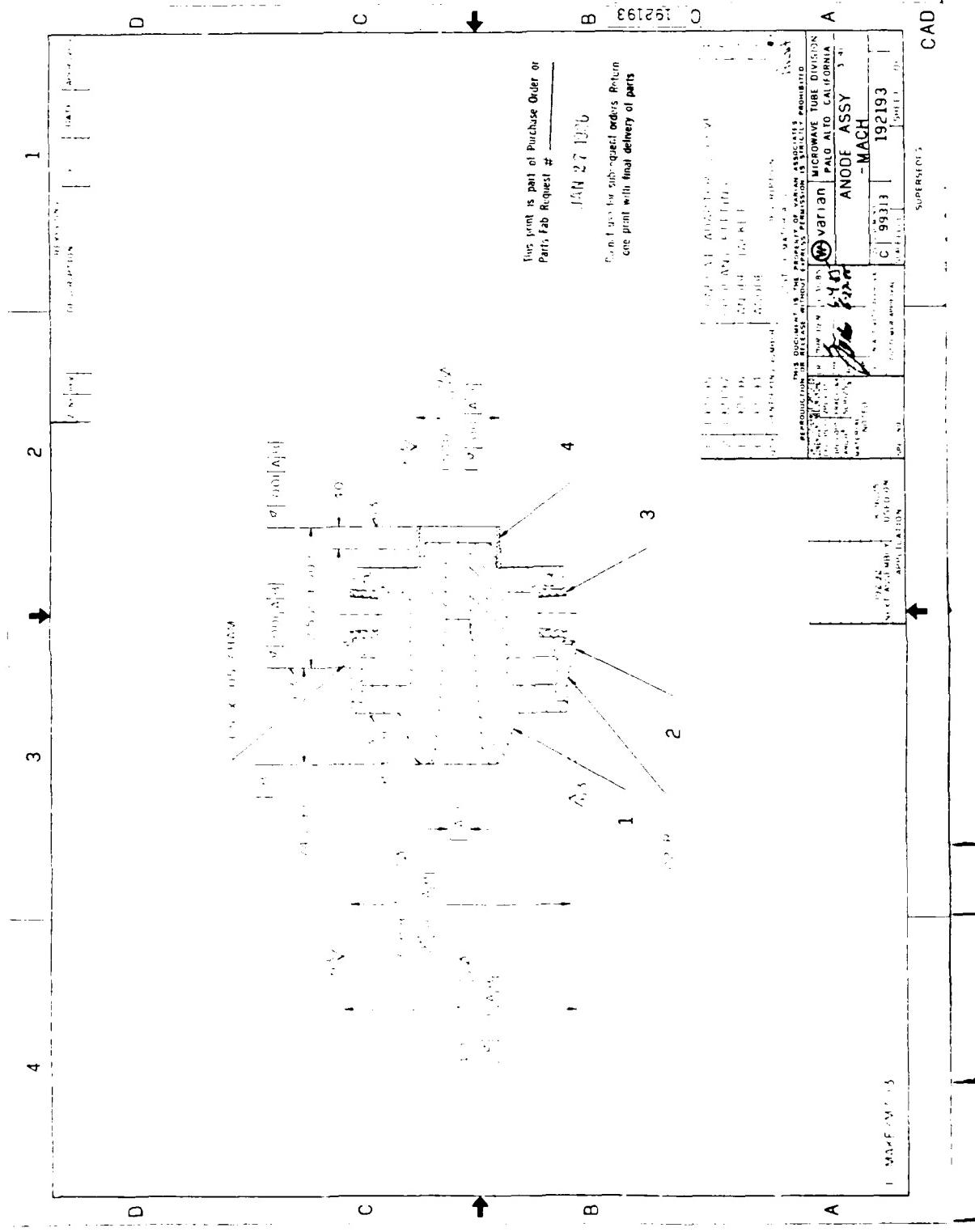
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JAN 27 1986							
Do not use for subsequent orders. Return one print with final delivery of parts.							
DETAIL A SCALE: 4/1							
ITEM _____ LIST OR MATERIAL _____ THIS DOCUMENT IS THE PROPERTY OF VARIAN ASSOCIATES REPRODUCTION OR RELEASE WITHOUT EXPRESS PERMISSION IS STRICTLY PROHIBITED DESIGNER: MARSDEN, JR. DATE: 1-29-85 REC'D.: 1-30-85 APPROV'D.: 1-30-85 IPI: 205 PARCHMENT ANGEL: 25V MATERI: 304 SST DESIGN ACTIVITY APPROVAL: 1-30-85 CUSTOMER APPROVAL: 1-30-85 SPEC NO: PI-38 192185 MATL ASSIST MARY USED ON APPLICATION							
FOCUS ELECTRODE 1/41 A							
CAD							

1	2	3	4	B	192192	C	D	A
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				REVISIONS				ECO DATE APPROVED
				DESCRIPTION				Part's Print is part of Purchase Order or Parts Fab Request # _____
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				192193				2 75Ø CONFLAT VA #954-5071
				IDENTIFYING NUMBER				ANODE ASSY - MACH
				MANUFACTURER				LIST OF MATERIALS
				6/1/85				THIS DOCUMENT IS THE PROPERTY OF VARIAN ASSOCIATES REPRODUCTION OR RELEASE WITHOUT EXPRESS PERMISSION IS STRICTLY PROHIBITED
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				PALO ALTO, CALIFORNIA				ANODE & CONFLAT ASSY
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				SPEC NO				SPEC NO 99313 - 192192
				APPLICATION				Subject to change or

CAD

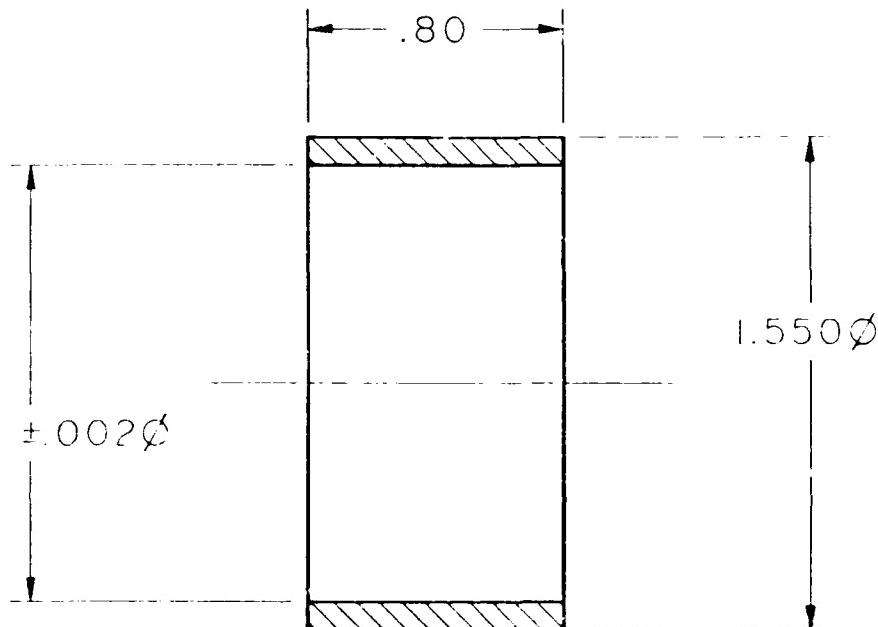


A 13



A 14

A 192195



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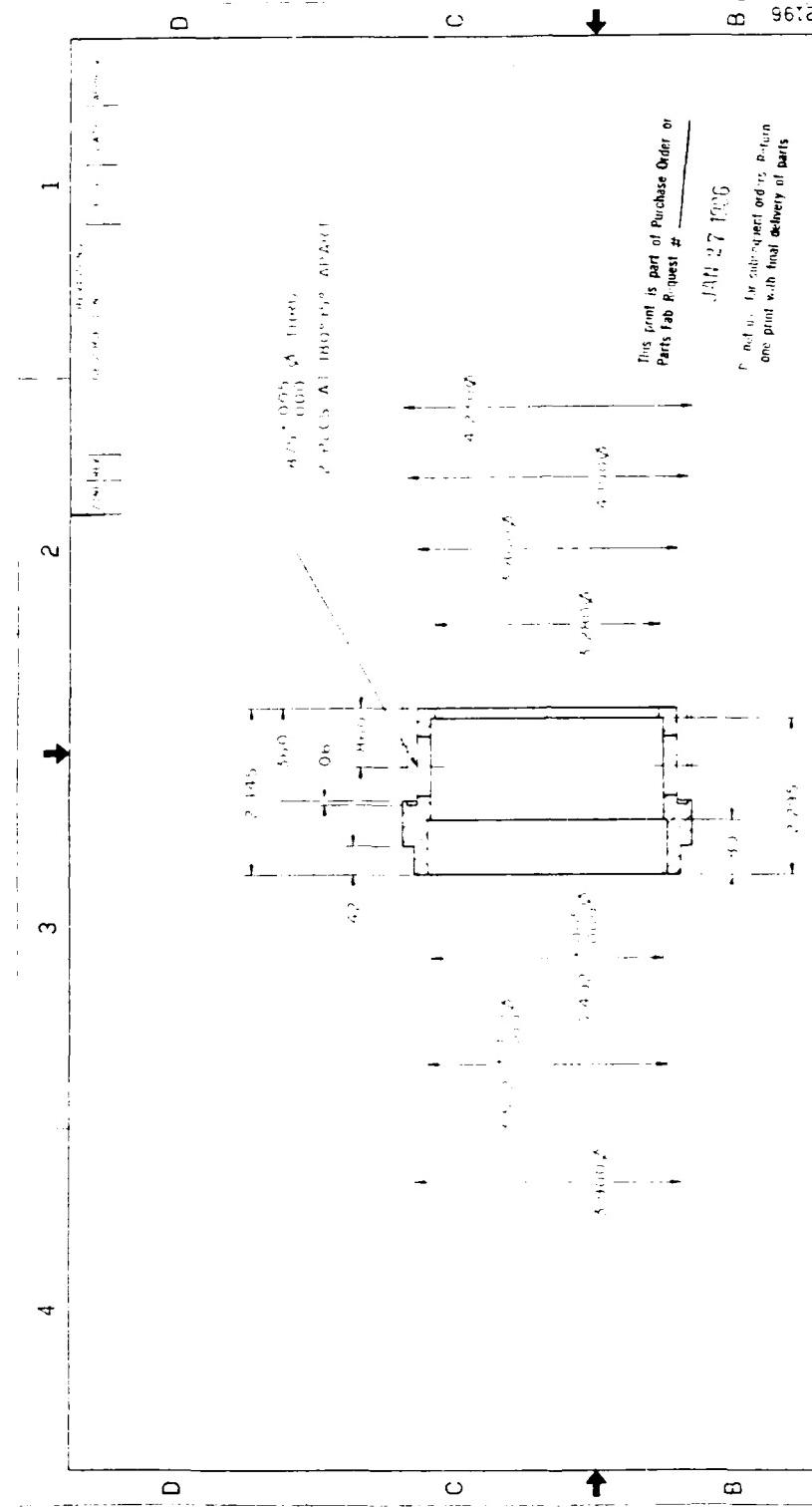
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JAN 27 1986

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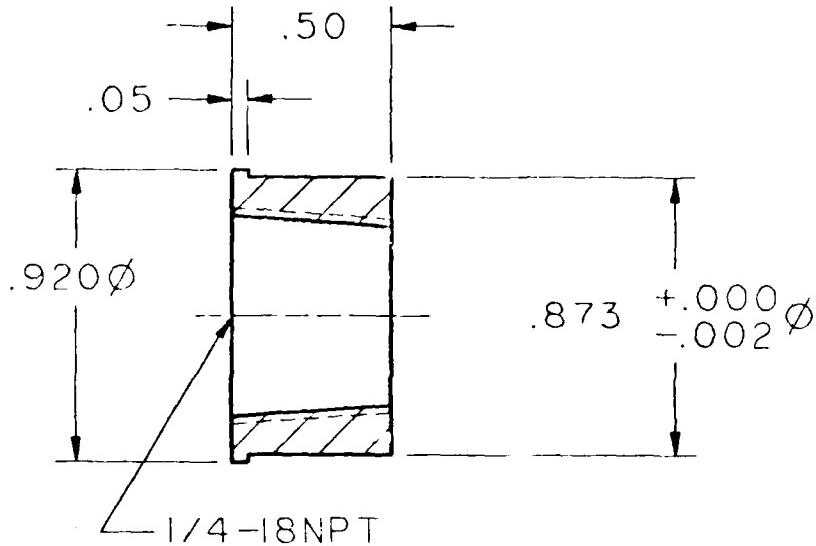
Do not use for subsequent orders. Return
one print with final delivery of parts

QTY	IDENTIFYING NUMBER	DESCRIPTION	ITEM
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DEC: IPL ± .11 2PL ± .02	CHK	5-30-85	MICROWAVE TUBE DIVISION PALO ALTO, CALIFORNIA
3PL ± .005 FRAC ± 1/64	APPD	5-27-85	
ANG ± 1° SUR125 ✓	APPD		
MATERIAL	CONFLAT ADAPTER SLEEVE		
304 SST TO FIN 1.555 OD MMC X 1.370 ID MMC	DESIGN ACTIVITY APPROVAL	SIZE A	FSCM NO. 99313
SPEC NO. PI-3D	CUSTOMER APPROVAL	SCALE 2/1	192195 SHEET OF
			3/41



A16

A | 192197



This print is part of Purchase Order or
Parts Fab. Request #

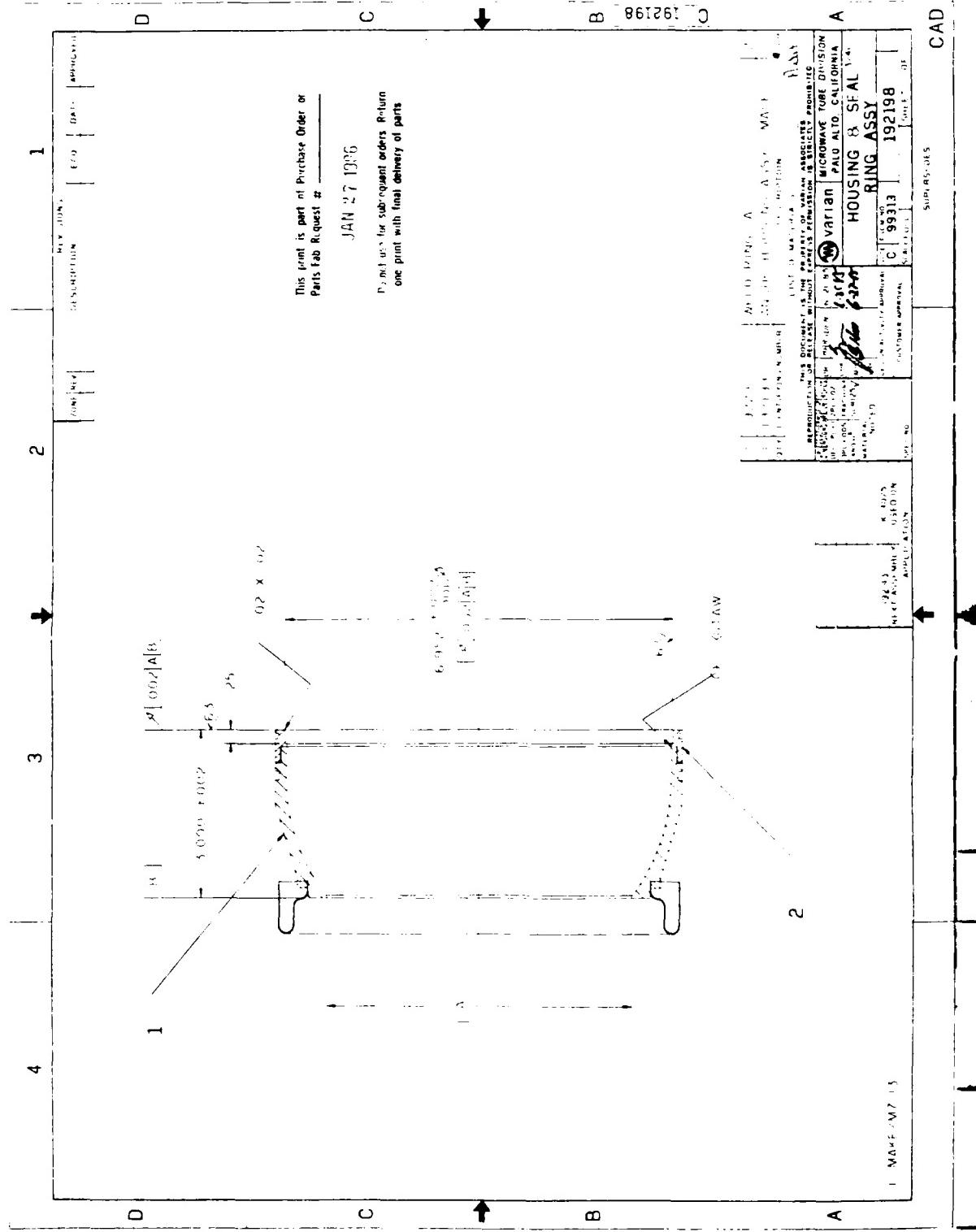
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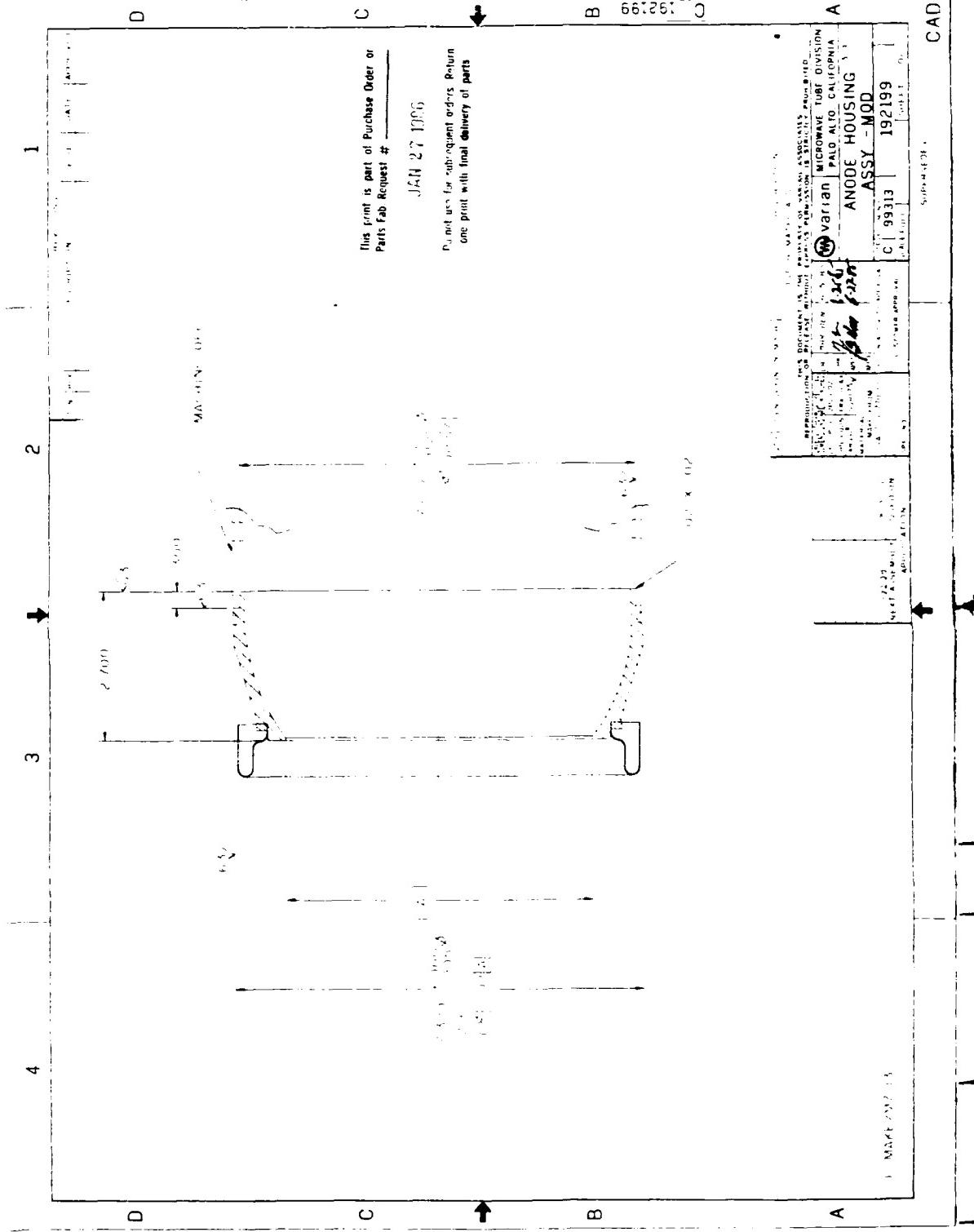
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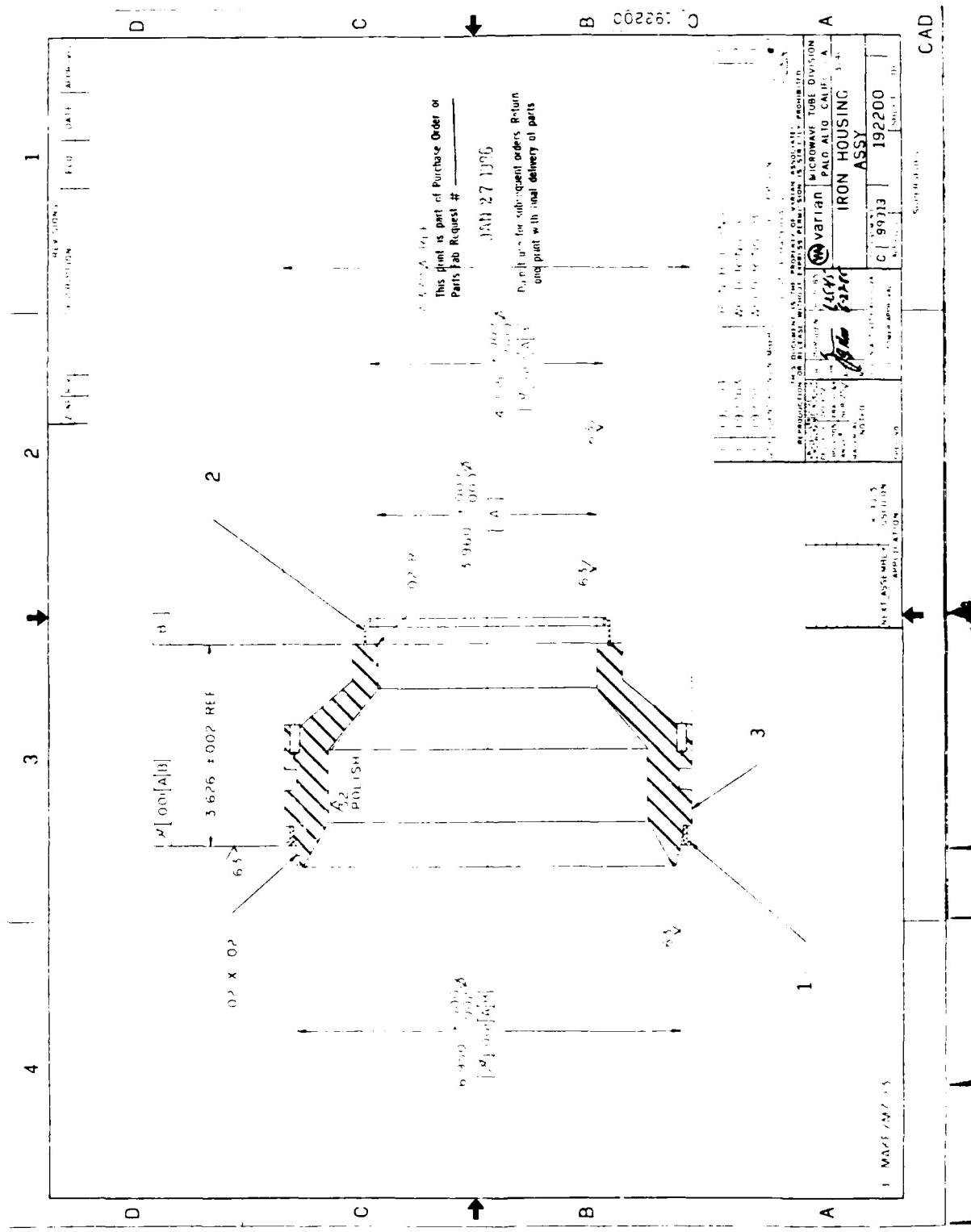
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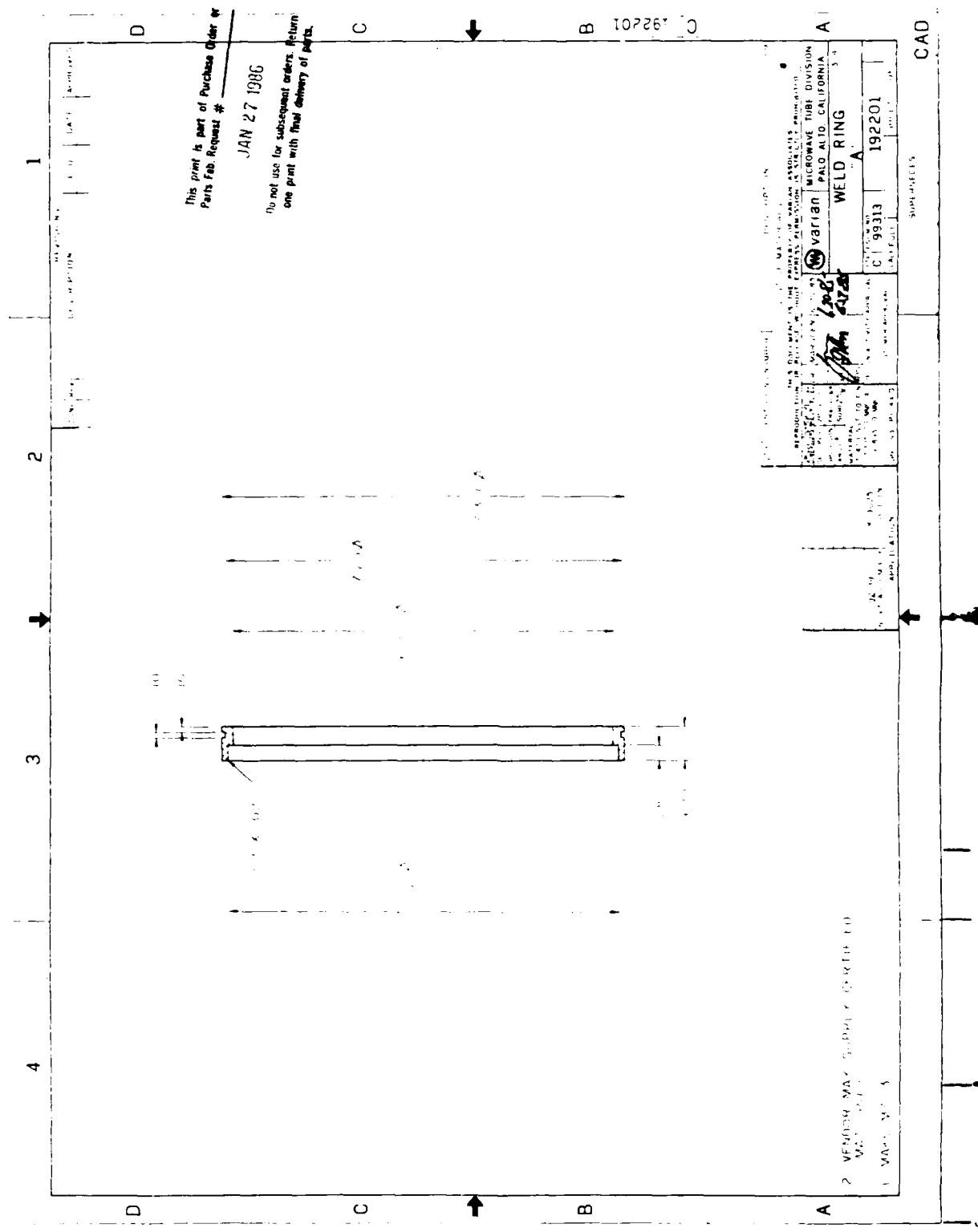
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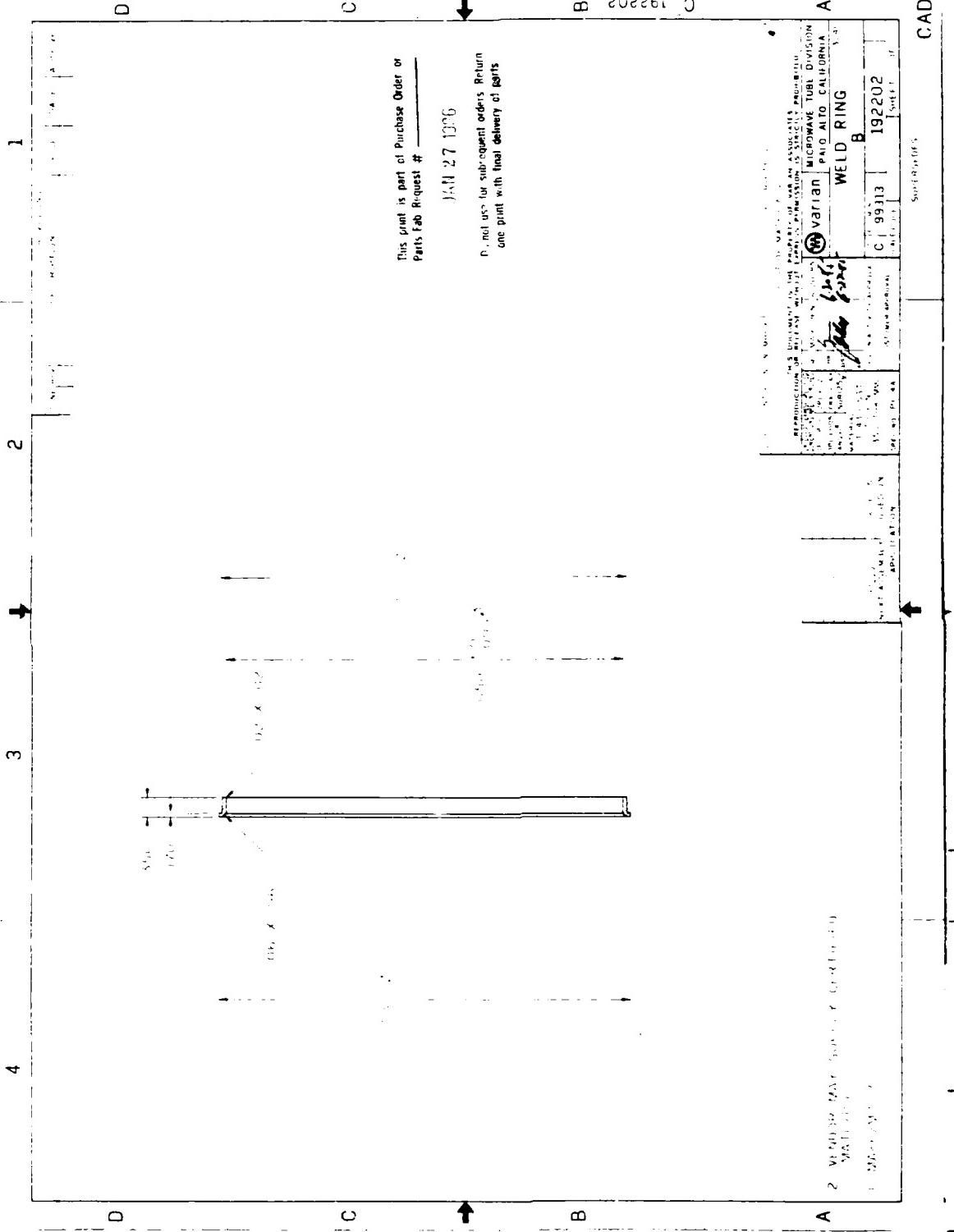
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DEC: ±PL ±.02		CHK		5-20-85	MICROWAVE TUBE DIVISION PALO ALTO, CALIFORNIA
3PL ±.005		FRAC: ±1/64			
ANG: ± [°]		SUR: 25/V			
MATERIAL		APPD		5-27-85	COOLANT FITTING 3/41
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SPEC NO. PI-3B		CUSTOMER APPROVAL			
		SIZE	FSCM NO.		
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		SCALE 2/1			SHEET OF

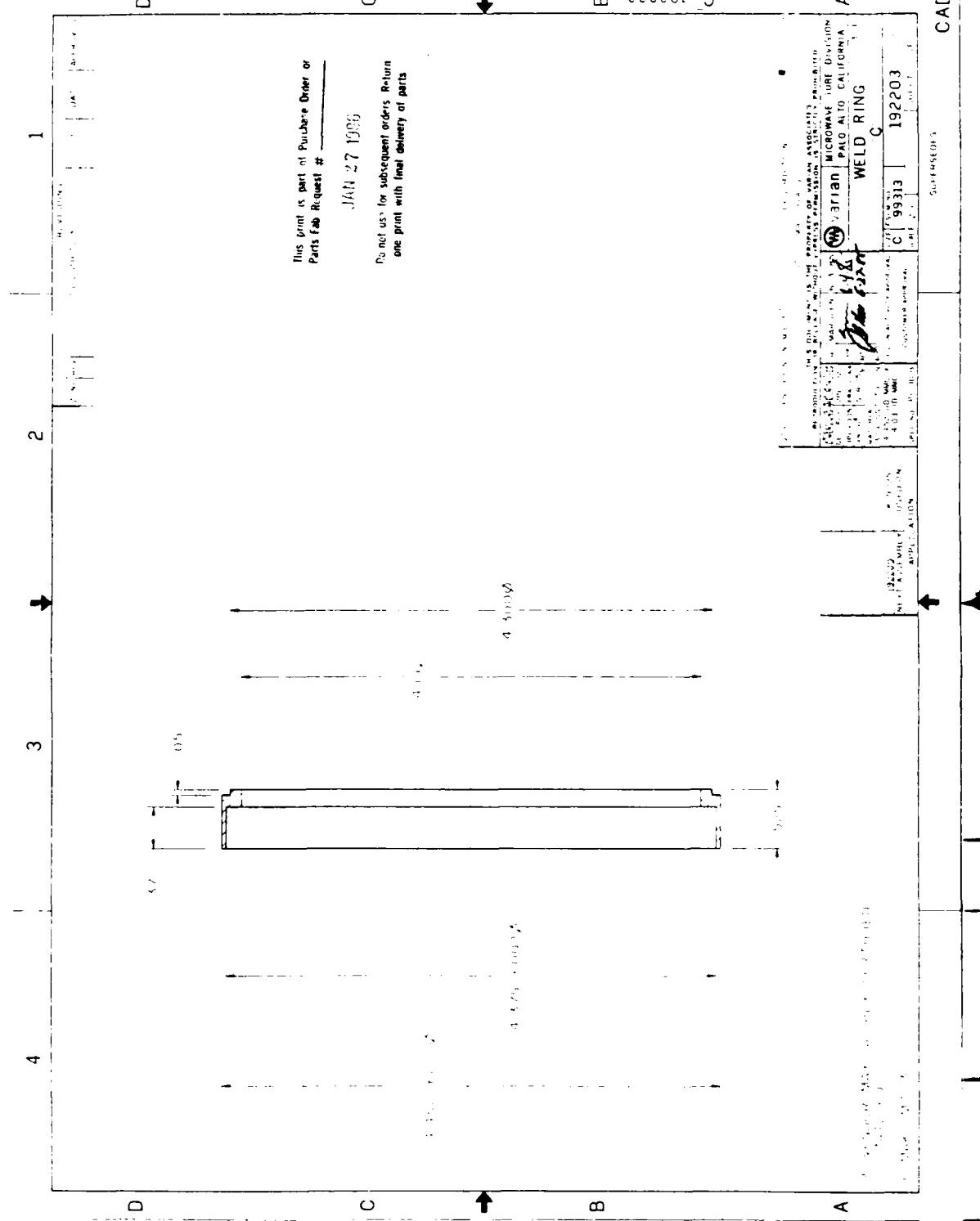


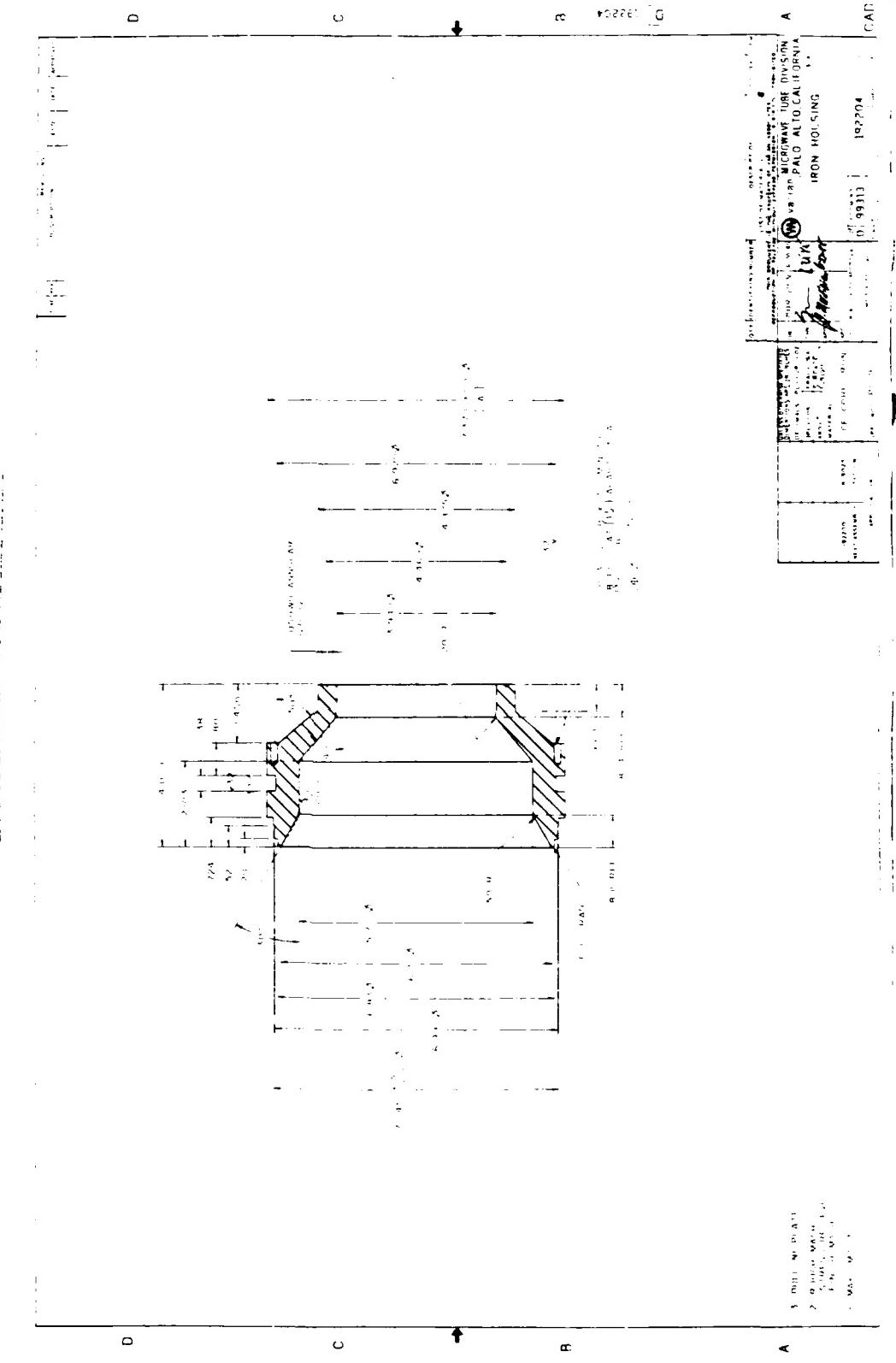




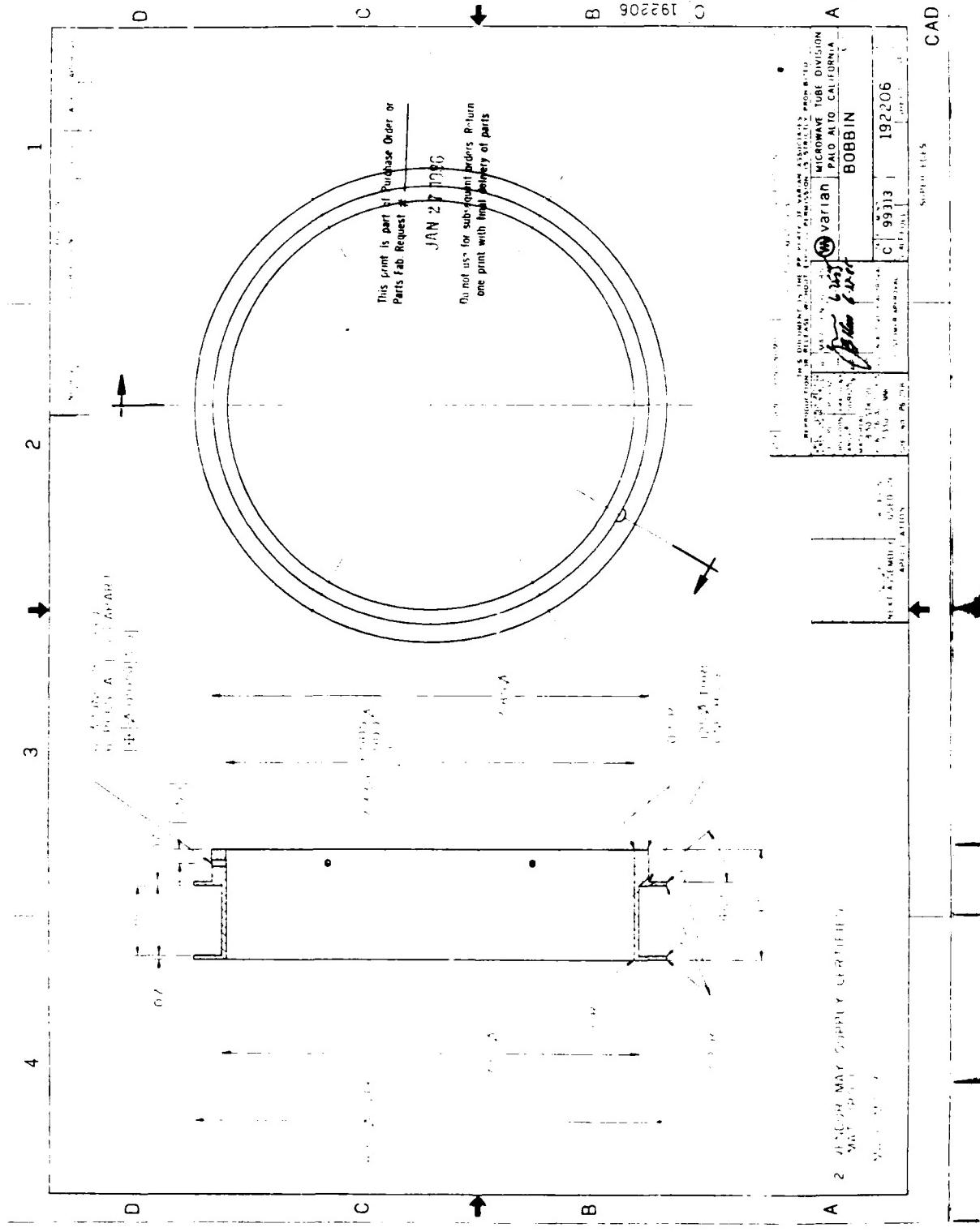


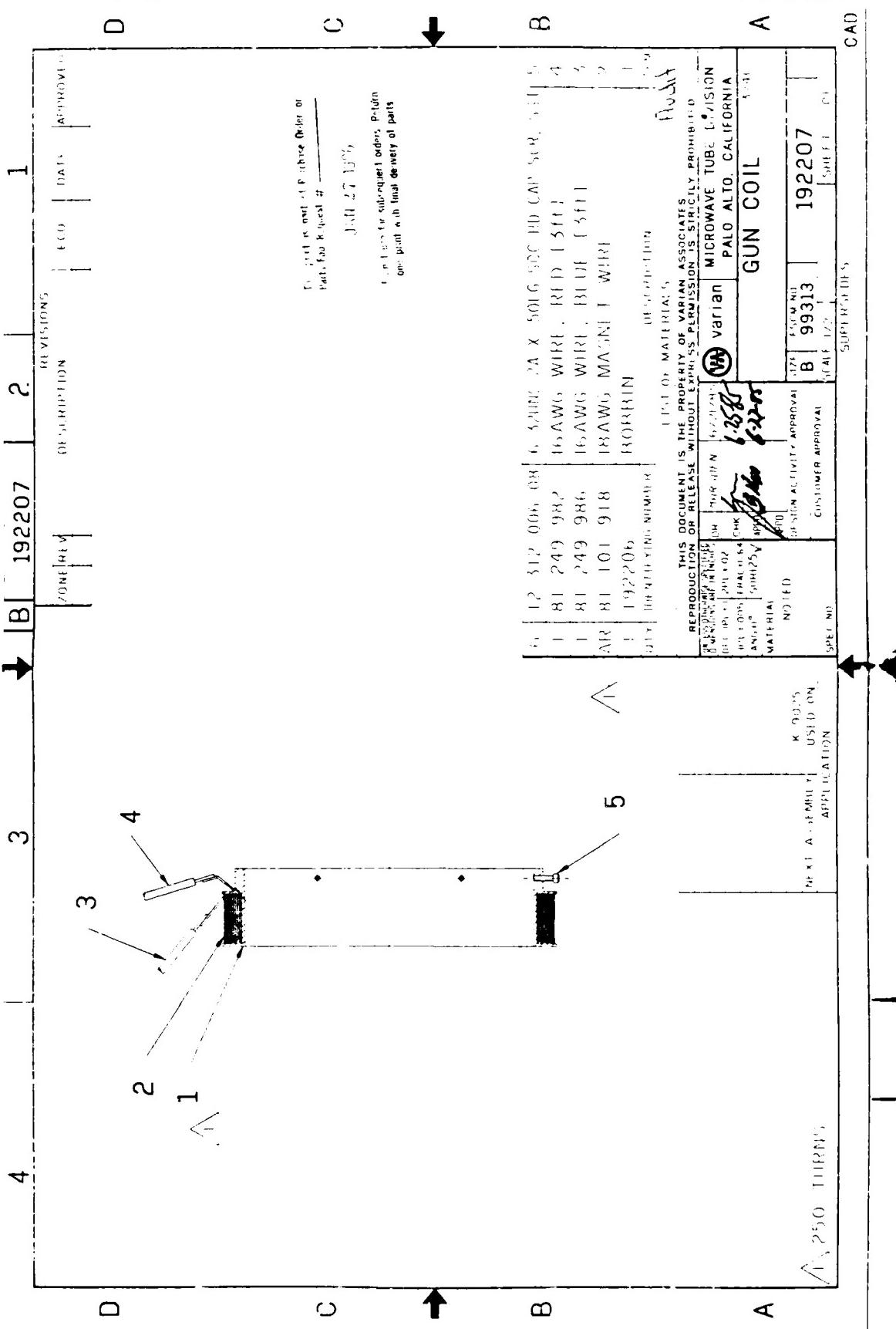


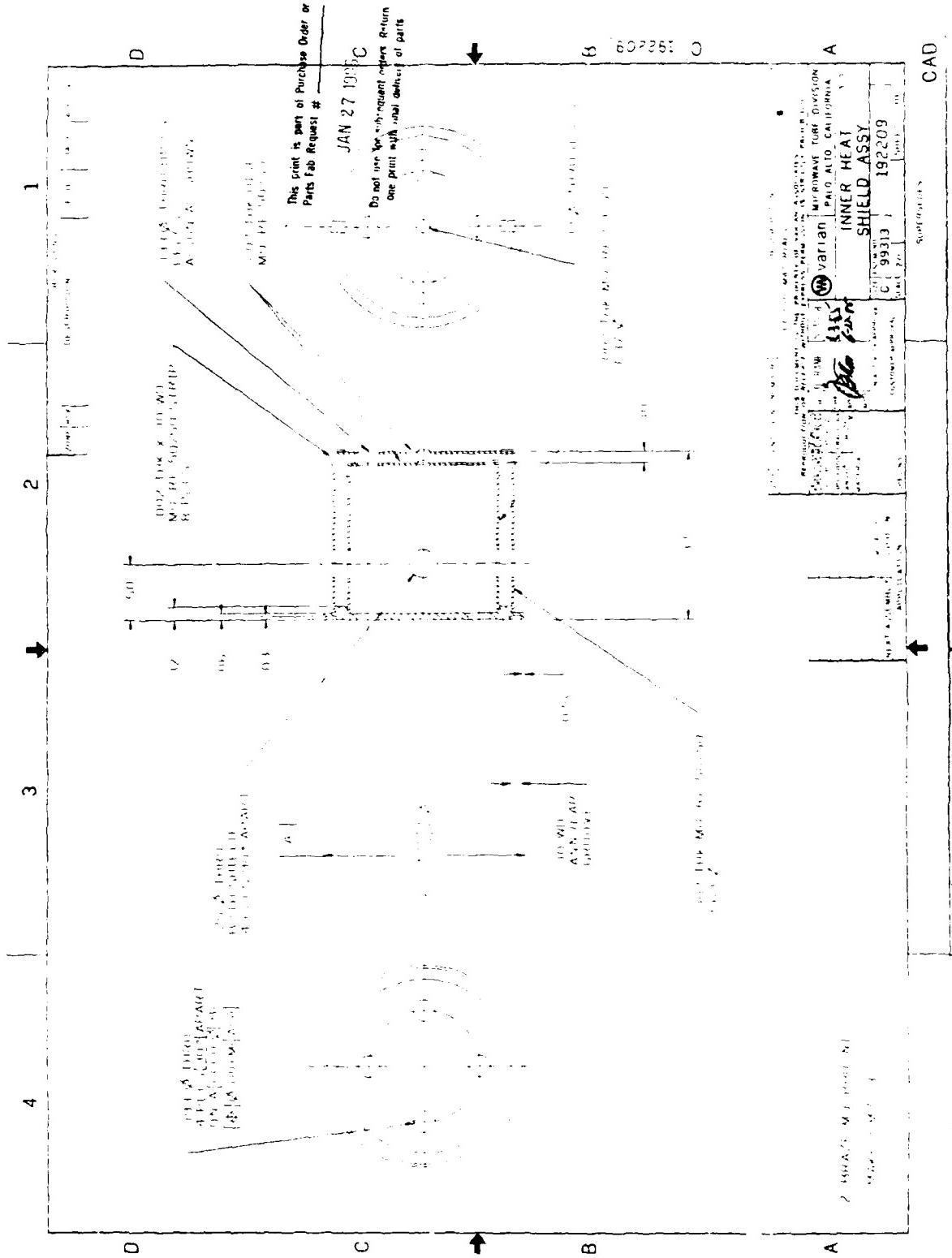


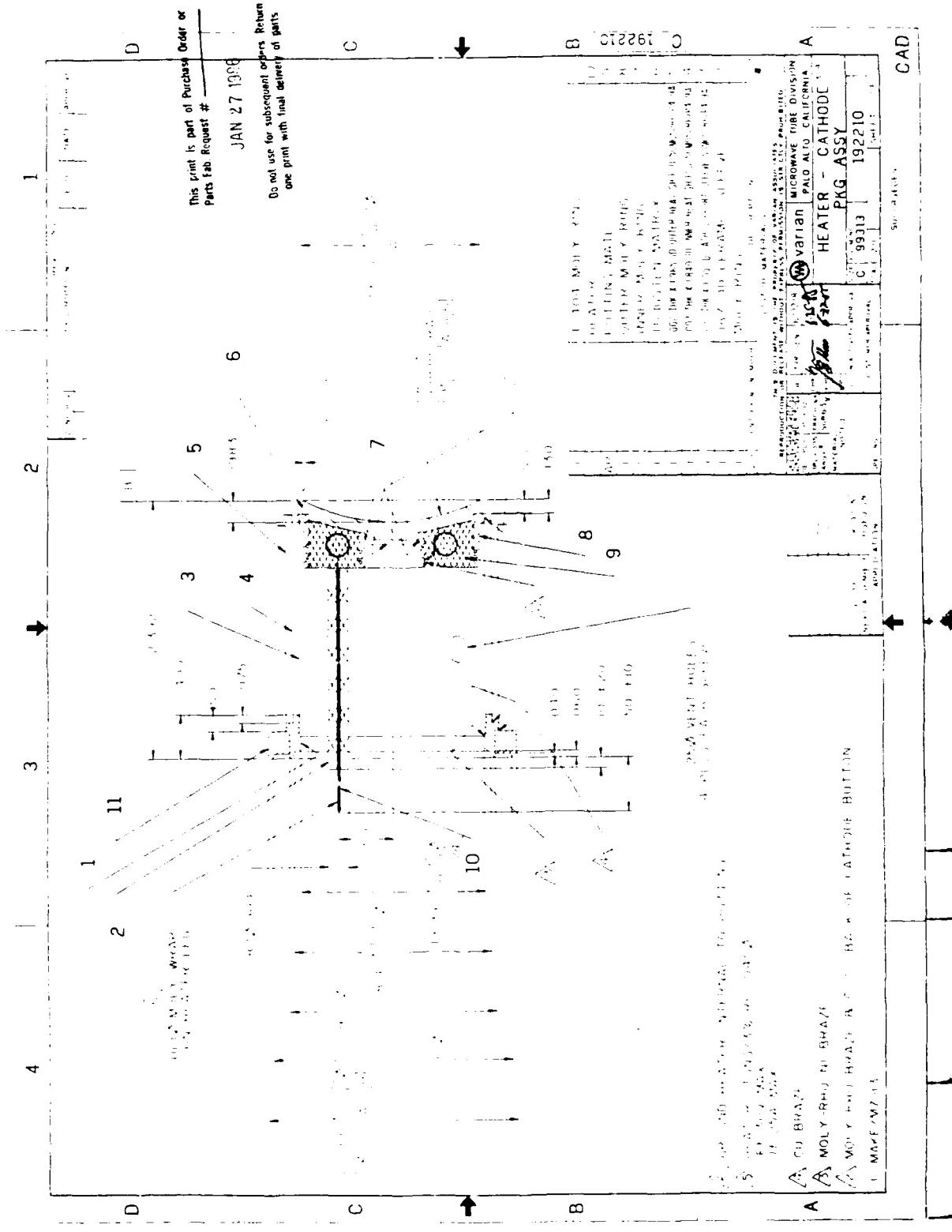


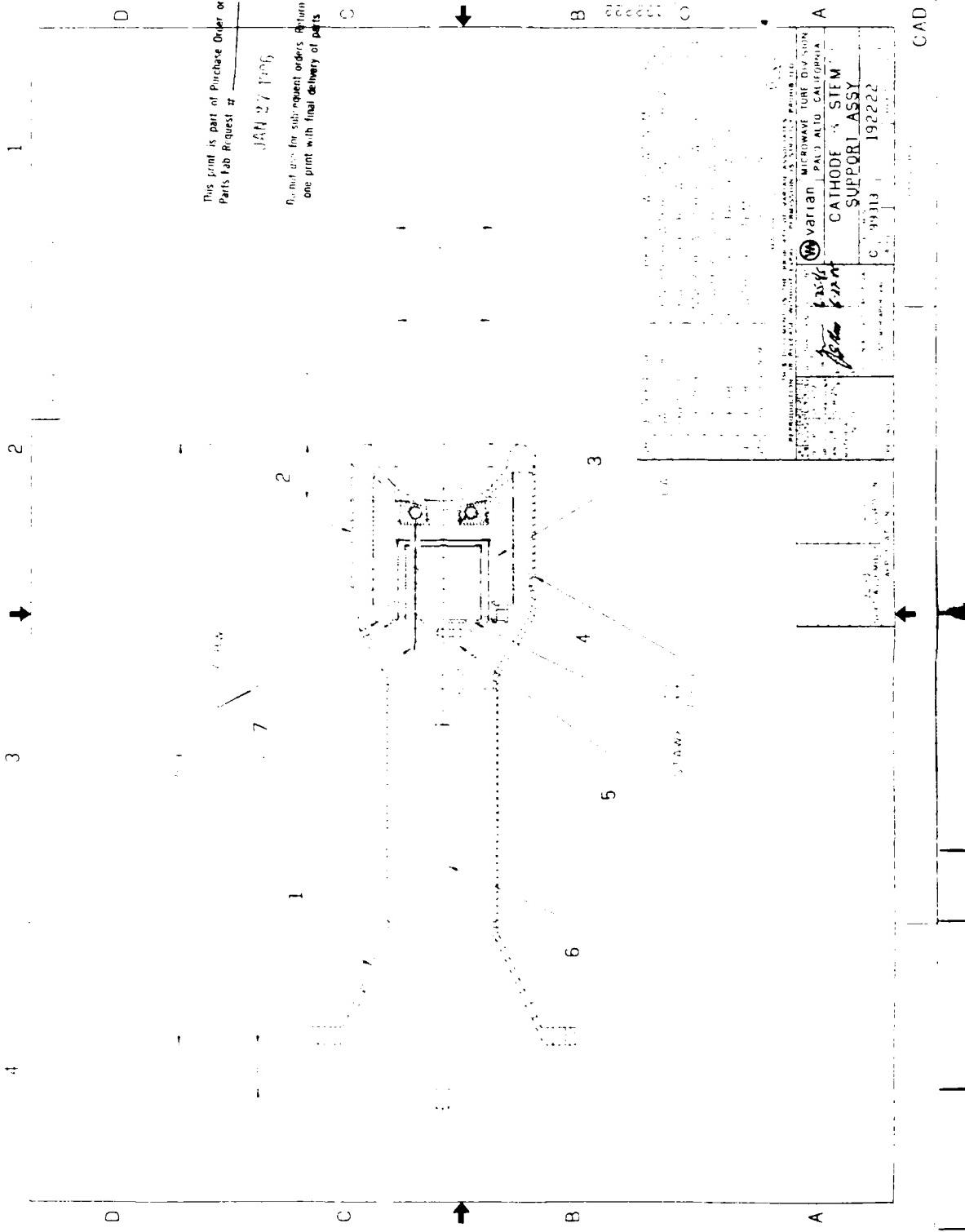
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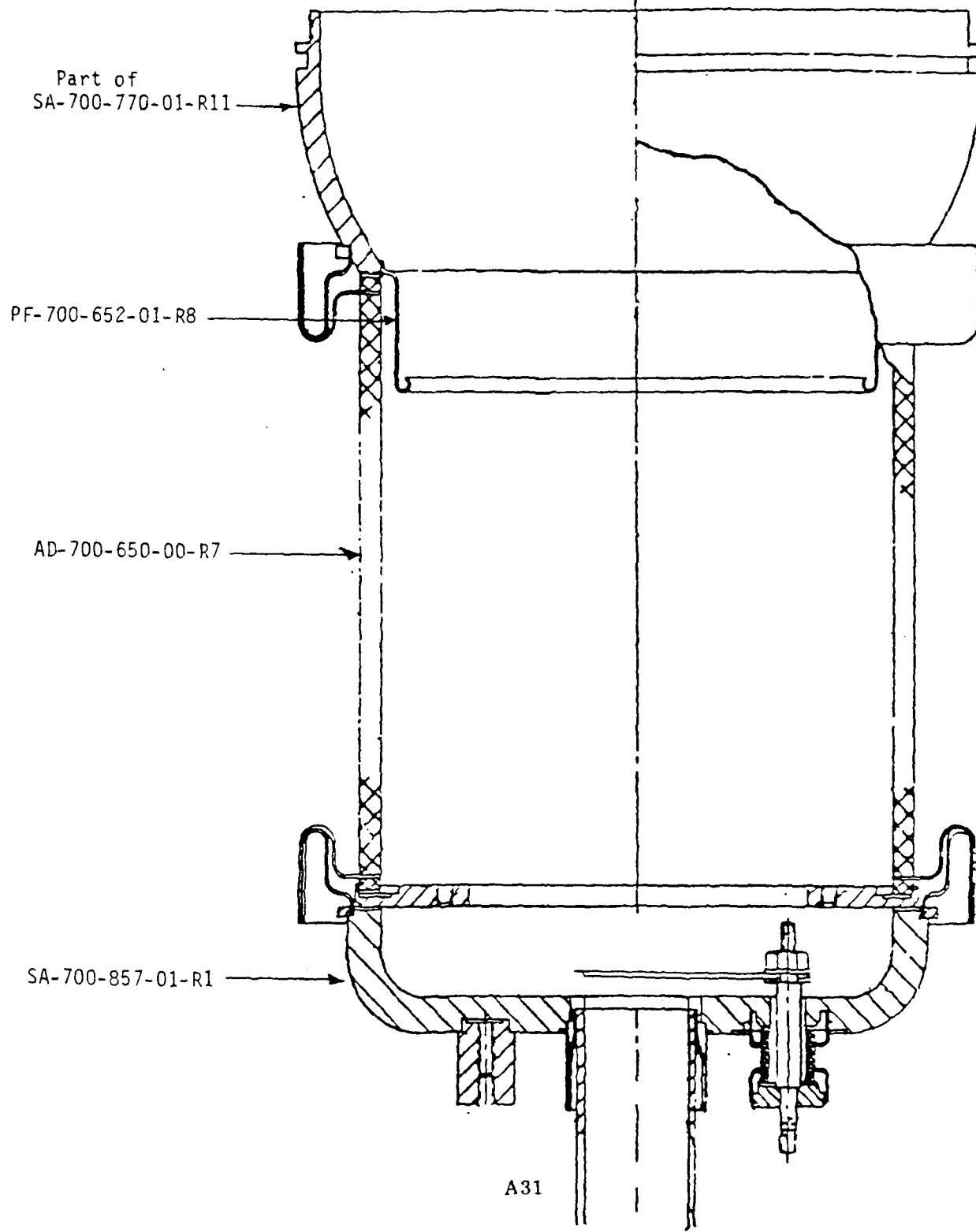






APPENDIX A-3
DETAIL PARTS DRAWINGS
(SLAC)

XK-5 SLAC GUN PARTS USED IN NRL GUN K-9025



XK-5 SLAC PARTS USED IN NRL GUN K-9025

<u>Title</u>	<u>Part No.</u>
Base-2 Gun Mount	PF-700-160-01-R8
Cath. Holdown Screw	212-01-R5
Ring Reinforcing	227-01-R6
Slip Ring	228-01-R7
Cylinder, Ctr. Heater	229-01-R9
Base Cup, Forming	287-01-R5
Cup, Base-finished	288-01-R15
Take-apart Joint-outer	297-01-R10
Anode Housing Blank	301-03-R10
Ring, Back Up	648-01-R5
Ceramic	649-01-R3
Assy, Seal-ceramic	AD-700-650-00-R7
Ring, Corona	PF-700-652-01-R8
Cup, Sealing-male	654-01-R7
Tube, Pumpout	655-01-R5
Housing, Anode	682-01-R15
Rod, Center Heater	759-01-R7
Assy, Anode Shell (Mach)	SA-700-770-01-R11
Asm. Ctr. Heater Cond.	783-01-R4
Assy Pumpout	857-17-R0
Ring, PL-back Up	PF-700-862-04-R0
Ceramic, Plated	862-05-R0
Assembly, Base Cup	SA-700-857-01-R1

#10-32 NF-2 THRU 4-HOLES
EQUALLY SPACED ON 1/25 DIA 8.

#10-32 NF-2 THRU 3-HOLES
AT 120° APART ON
5/32 DIA B.C.

PF-700-160-01-RB

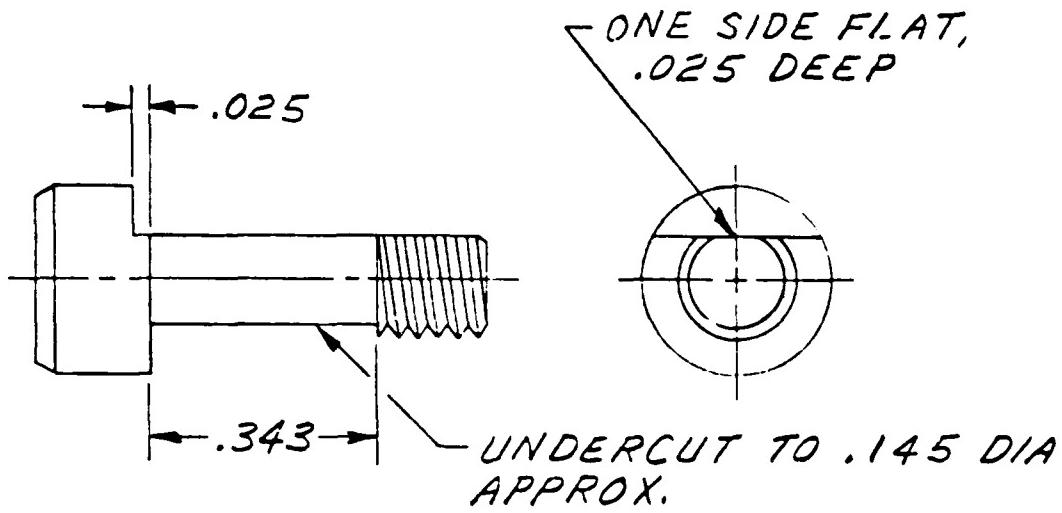
This technical drawing illustrates a mechanical assembly with various dimensions and tolerance specifications.

- Left Side:** A vertical slot has a width of $.218$ and a tolerance of $\pm .002$, labeled as **A**.
- Middle Section:** A horizontal slot has a width of 6.060 and a tolerance of $\pm .015$, labeled as **B**.
- Bottom Left:** A dimension of 5.25 is shown with a tolerance of $\pm .005$.
- Bottom Center:** A dimension of 3.625 is shown with a tolerance of $\pm .015$.
- Bottom Right:** A dimension of 6.015 is shown with a tolerance of $\pm .015$.
- Bottom Left Angle:** An angle of 15° is indicated.
- Right Side:** A vertical slot has a width of $.090$ and a tolerance of $\pm .015$, labeled as **-A**.
- Bottom Right:** A dimension of $.060 \times 4.5$ is shown with a tolerance of $\pm .015$, labeled as **-A**.

A33

NOTE:

1. MATT'L: #304 STN STL
2. STRESS RELIEVE AT 950-1000 °C. FOR 10-20 MIN.
3. USE ONLY SLAC APPROVED MACHINING FLUIDS PER SC-700-286
4. NEXT ASSY: AD-704-01-00



NOTE:

1. MADE FROM ST'D #10-32 NF-2 X 1/2 LG.
SOC HD CAP SCR, #304 STN STL
2. USE ONLY SLAC APPROVED MACHINING FLUIDS
PER SC-700-B66-47.
3. NEXT ASSY: AD-704-011-00

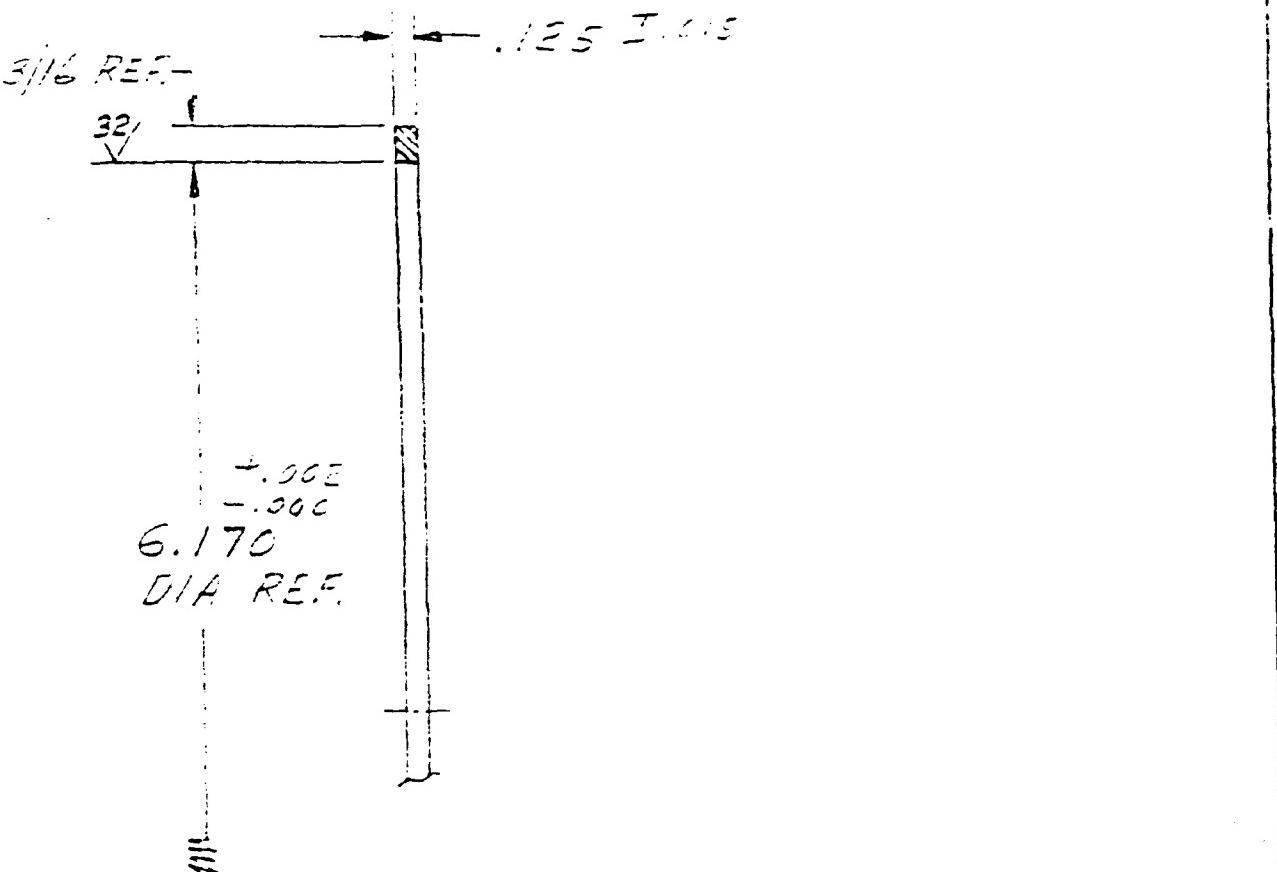
1. DRAWN BY
2. MFG BY
3. DATE
4. APPROVAL
5. APPROVAL

SCALE: 4" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R3	REDRAWN & REVISED	H.G.	6-6-72	S.E.	6-7-72
R4	CHG. TITLE	B.E.	11-15-70	RTH	11-15-70
R5	ADDED NOTE 2&3	J.G.	12-30-75	RTH	1/11/84

STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY		CATH HOLDOWN SCREW XK-5 KLYSTRON	
ENGR DPTS CNC	R. CALLIN H. GREENBAUM 11-15-70	APPROVALS V. J. HALL C. T. COLE	PF-700-212-01-R5 A

11/11/85



NOTE:

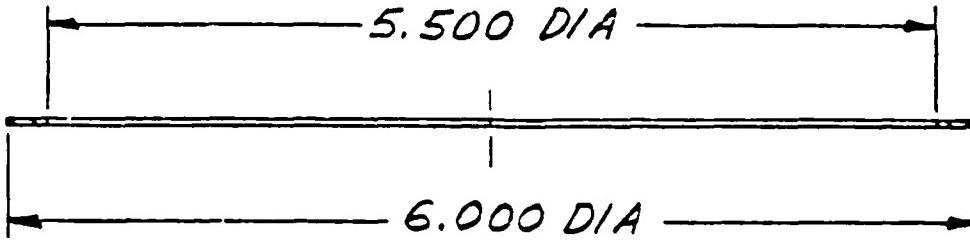
1. MADE FROM PF-700-768-01

UNLESS NOTED
TOLERANCES BREAK CORNER C/S
FRONT = 1/64 ~~BACK = 1/32~~
REC. = 0.05
ANGLE = 1/12° 63

SCALE: 1" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R2	REVISED & REERAWN	H.G.	10-13-67	1PM	10-13-67
R3	.032 X .032 BRAZE GROOVE WAS .042 X .042	H.G.	11-28-67	A.S.	11-28-67
R4	CHG. TITLE	H.G.	8-19-70	KLC	8-19-70
R5	CHG. TITLE	H.G.	11-16-70	F.F.I.	11-16-70
R6	DEL. BRZ. GROOVE	SS	1-22-80	H.G.	1-22-80

STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		RING, REINFORCING XK-5 KLYSTRON	
ENGR. <u>P. STRINGALL</u> DPS. <u>H. GREENHILL</u> CMC <u>D.W.</u>	APPROVALS <u>10-13-67</u>	PF-700-227-01-R6	A



NOTE:

1. MAT'L: .005 OR .007 MOLYBDENUM
2. CHEMICAL CLEAN BEFORE PUNCHING
3. NEXT ASSY: AD-704-011-00.

SCALE: 1" = 1"

LINER NO. 200
TOLERANCES BASED ON DRAWINGS
FACT ± 1/64 INT. RAD. ± 0.05
DEC ± 0.05 63
ASSEMBLY ± 1/16 Y

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
P3	REDRAWN & NOTE 2 ADDED	H.G.	12-2-69	R/C	12-2-69
R4	CHG. TITLE	H.G.	6-19-70	R/C	6-19-70
R5	CHG. TITLE	L.E.	11-1-70	R/C	11-1-70
R6	CHG .007 TO .005 OR .007	S.S.	2-22-80	H.G.	2-22-80
R7	ADDED NOTE 3	J.G.	12-22-83	R/TAD	12-22-83
STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		SLIP RING XK-5 KLYSTRON			
ENG'D R. CALLIGR. D/PIS H. GREENHILL CNC P.L. 252	APPROVALS PL 12-2-69	PF-700-228-01-R7 A			

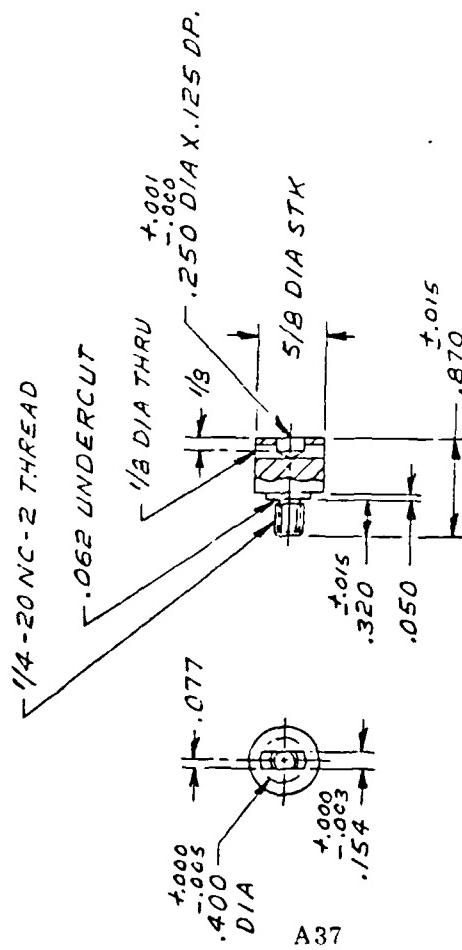
12-2-69

A36

MRF7

B 7-10-622-00L-PD

REV	DESCRIPTION	DRN.	CART	APP	DATE
F9	P.DRAWIN & ADDED NOTE 1.	M.G. 17/8/63 R.713	4/26/64		



NOTE:
1. USE ONLY SLAC APPROVED MACHINING
FLUIDS PER SC-700-866-47

304 L STV STL			
ITEM NO	PREFIX	BASE STOCK OR PART NO	SUFFIX
DO NOT SCALE DRAWING			TITLE OR DESCRIPTION
			NEXT ASSEMBLY SA-700-783-C1
SCALE : " = "			
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES: OPEN EDGES OOS-0.015 INTERNAL CORNERS: OIS OR MAX FRACTIONS: 1/8, 1/4, 1/2, 5/8, 3/4 DEC.: .000, .001, .002, .003, .004, .005 ANGLES: 1/2°, 3/4°, 1/2, 3/4, 1/2, 3/4, APPROX			
STANFORD LINEAR ACCELERATOR CENTER U.S. DEPARTMENT OF ENERGY STANFORD UNIVERSITY STANFORD, CALIFORNIA MAY 1964			
PP-700-229-01-R9 B			
SH - CF			M/F/N?

1. DRAWN BY: T.G. 2. DATE: 7-17-76 3. TITLE: BASE CUP FOR XK-5 KLYSTRON 4. SCALE: 1" = 1" 5. MATER: 3/8 THK. CERT OF HC CU. PLATE				
NOTE: 1. SEE PF-700-288 FOR MACHINING INFORMATION 2. BLANK SIZE = 7 7/8 RD., SAW CUT & MACHINE TO 7.750 $^{+.000}_{-.015}$ 3. ANNEAL AT 750 - 800°C. FOR 15 MIN. BEFORE FORMING				
SCALE: 1" = 1"		MAT'L: 3/8 THK. CERT OF HC CU. PLATE		
REV.	DESCRIPTION	DRN.	DATE APP.	DATE
R2	REDRAWN & NOTES 2 & 3 ADDED	H.G.	7-17-76	11-16-76
R3	CHG. TITLE	H.G.	5-18-76	11-16-76
R4	CHG. TITLE	H.G.	11-16-76	11-16-76
R5	REV. NOTE: 3.	H.G.	12-21-85	11-16-76
STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY		BASE CUP, FORMING XK-5 KLYSTRON		
INGR: R. CALLIN DTGS: H. GREENHILL CHE:		APPROVALS 7-17-76		PF-700-287-01-R5
				A

REV.	DESCRIPTION	DIN	CATE.	APR.	DATE
R-3	RECDRMIN	S.S	ENCL	H.G.	2-25-71
A-14	ADDED ACC. ON S. 360 24-10	J-1	PROJ.	H.G.	3-1-71
R-15	ADDED 6EAM. TOWER - REVISED NOTE 3	J-6	PROJ.	H.G.	3-1-71

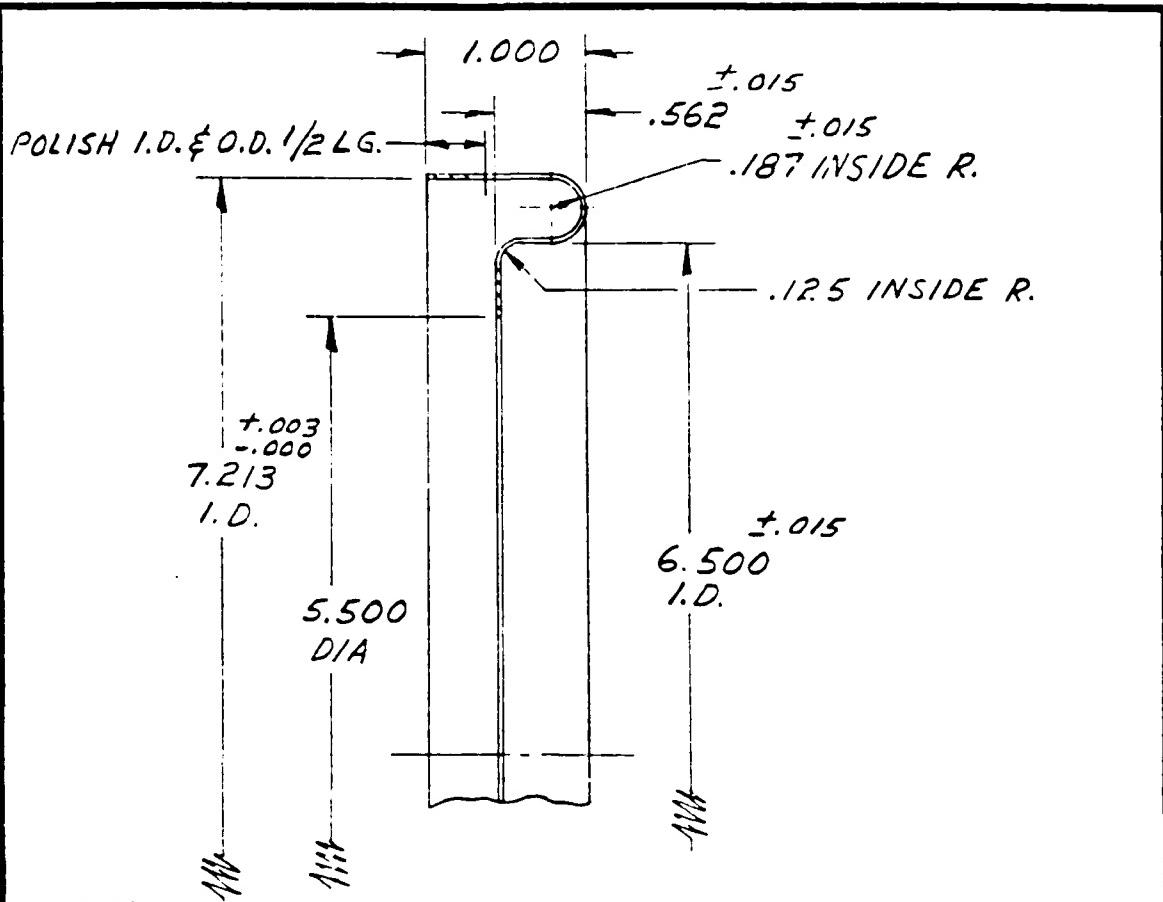
- 250 DIA THRU
#-PIECES AT 90° APART
D.N. 1.125 DIA B.C.
- 1.125 DIA THRU 1.300 DIA
X.260 D.D., 1.502^{.002}, 1.502^{.002} DIA
X.125 D.D., 1.687^{.002} DIA X
X.032 D.D.

1.125 DIA THRU : .3000 DIA
 X .250 DIA, 1.50² + .005 DIA
 X .125 DIA, 1.687 DIA
 .032 DIA.

NOTE:

1. MANDREL FROM PT. 700-257-01
2. ALL MACHINED SURFACES 32
3. USE ONLY SLAC APPROVED MACHINING FLUIDS P.F.R. S.C. 700-26G-47.

THE ST. VINCENT'S HOSPITAL FOR THE MENTALLY ILL,
NEW YORK CITY, RECEIVED A GRANT OF \$10,000.00 FROM
THE ST. VINCENT'S FOUNDATION.



NOTES:

1. BLANK SIZE = 10 1/3" ROUND BLANK.
 2. USE ONLY SLAC APPROVED MACH. FLUIDS PER SC-700-866-47
 3. NEXT ASSY: AD-700-650-00.

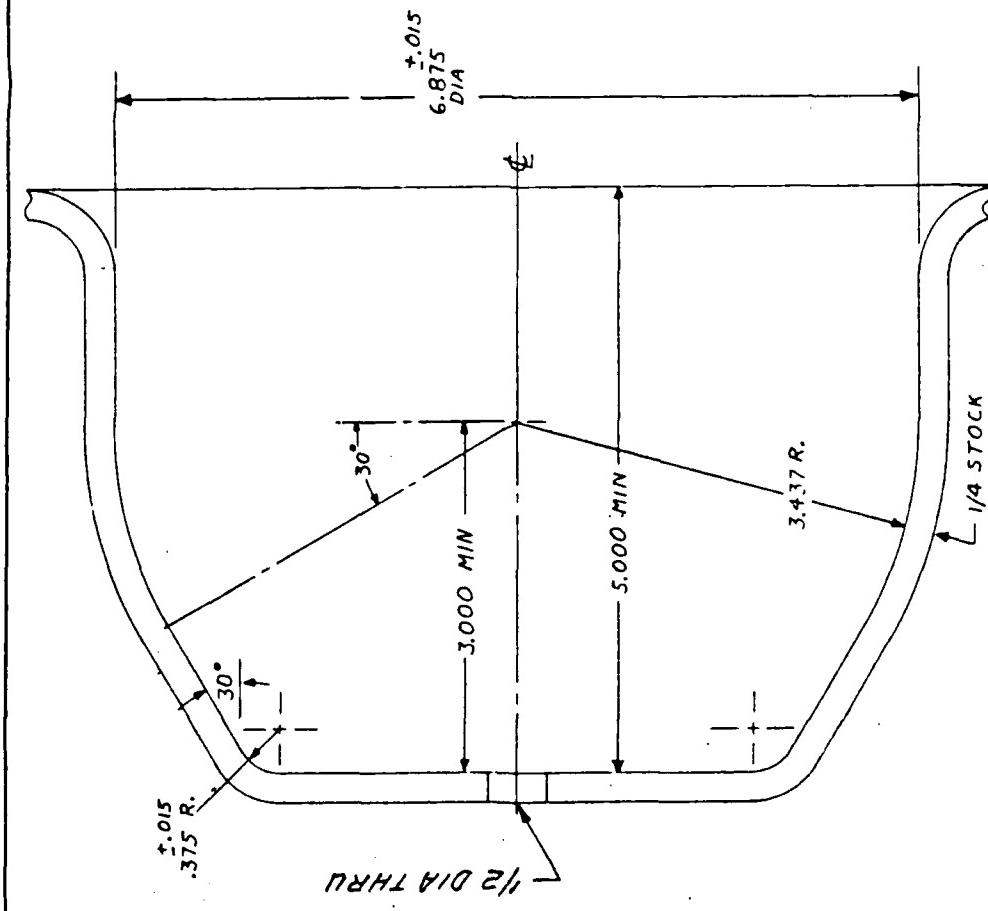
UNLESS NOTED
TOLERANCES DRAFTS COUNTERS .005
.001-.005 .001-.005 .005
.001-.005 .001-.005 .005
.001-.005 .001-.005 .005

R7	ADDED POLISH NOTE	9-13-78 H.G.	18
RC	CHG. TITLE	11-15-78 C.P.	1
RS	CHG. TITLE	3-18-79 H.G.	LL
R4	BLANK SIZE WAS 12" SQ.	12-14-78 H.G.	1
R13	ADDED NOTE 2. - E	12-21-78 P.M.	RTA
PS	DEL. NOTE 2.	12-9-78 H.G.	11
RE	ADDED NOTE 2.	9-17-79 H.G.	1

STANFORD LINEAR ACCELERATOR—M U. S. ATOMIC ENERGY COMMISSION		TITLE TAKE-APART JOINT-OUTER XK-11 KLYSTRON	
MAT'L. .CE 3 THK. 75-50 CUPRO-NI			
ENGR. <u>WILLIAM J. HILL</u>	CHK'D. <u>10/15/63</u>	DATE <u>10-10-63</u>	
DFTS. <u>WILLIAM J. HILL</u>	APP'D. <u>10/15/63</u>	SCALE <u>1" = 1"</u>	PF-700-297-01-R10

B 01R-10-102-00L-Fd

REV	DESCRIPTION	DRN	DATE APP	DATE
A/10	WAS MP-700-301-01, ADDED SPECS	H.G.	12-14-62	1-1-63

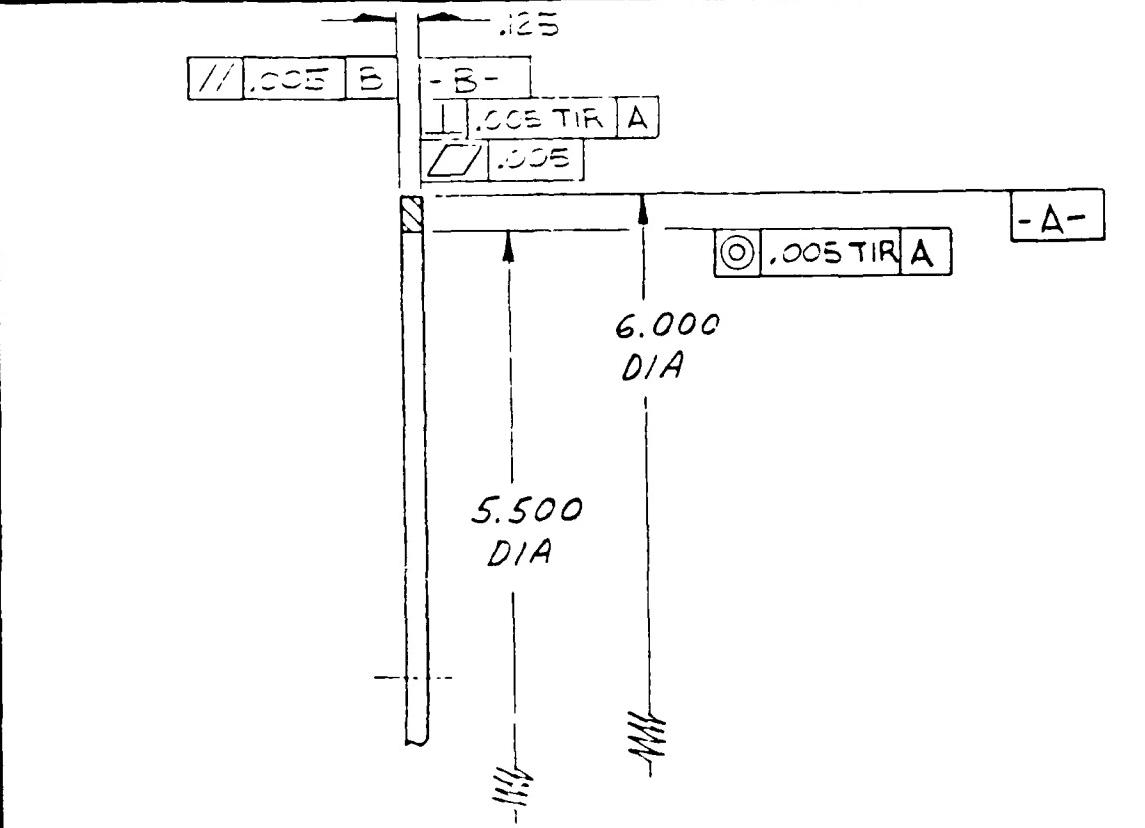


NOTE:
1. MATT'L: #304 STN STL, BLANK SIZE = 16" SQ.
2. STRESS RELIEVE AT 950° - 1000° C. FOR 10.
20 MIN. WITH FAST COOL

SCALE: 1" = 1" DO NOT SCALE DRAWING NEXT ASSEMBLY:

UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES	STANFORD LINEAR ACCELERATOR CENTER USE LINEAR RESEARCH AND DEVELOPMENT ADMINISTRATION STANFORD UNIVERSITY	APPROVAL
TOOLMARKS, SPOT FACES, DED. TOLERANCES TOLERANCE = 1/16 INCHES MAX. / .005 INCHES MIN.	FOR: G. KORNBLAD DATE: 1-1-63	APPROVED H. G. GREENWELL 1-1-63
ALL Holes 1/4" dia. V	REVIEWED A. H. COOPER 1-1-63	REVIEWED H. G. GREENWELL 1-1-63
ANCHRS 1/2" dia. V	INITIALS A. H. COOPER 1-1-63	INITIALS H. G. GREENWELL 1-1-63

PF-700-648
 879

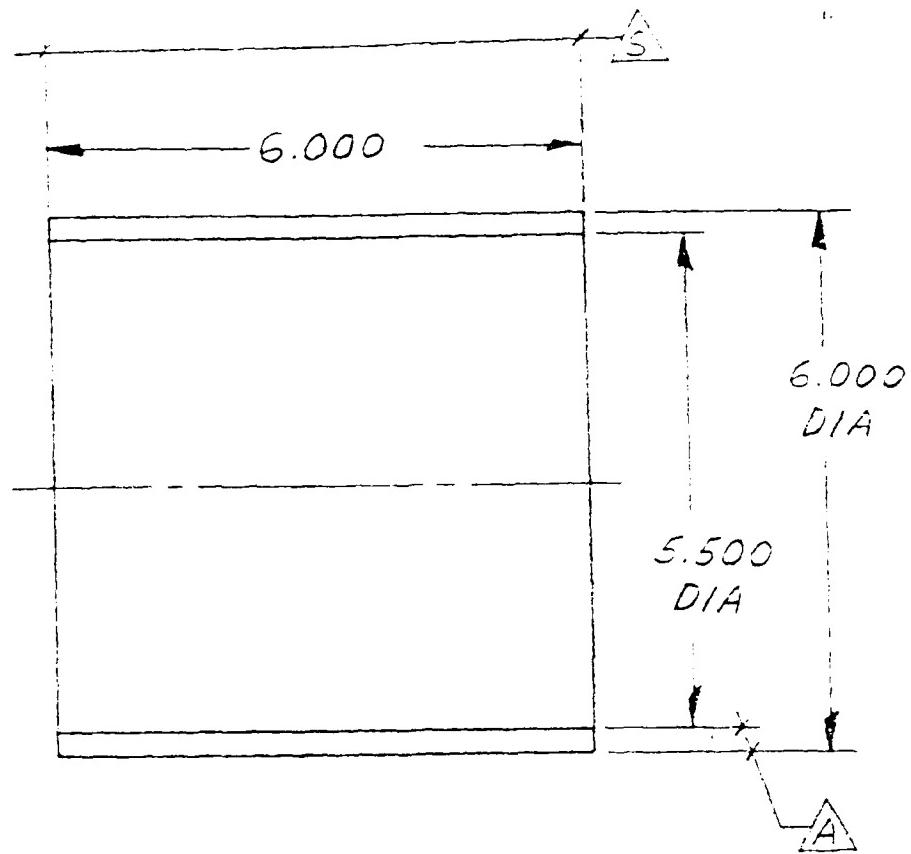
	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 30%;">11.005 B</td> <td style="width: 40%; text-align: center;">.125</td> <td style="width: 30%;"></td> </tr> <tr> <td>- B -</td> <td></td> <td></td> </tr> <tr> <td>.005 TIR A</td> <td></td> <td></td> </tr> <tr> <td>.005</td> <td></td> <td></td> </tr> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 30%; text-align: right; padding-right: 5px;">6.000</td> <td style="width: 40%; text-align: center; padding: 5px;">DIA</td> <td style="width: 30%;"></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">5.500</td> <td style="text-align: center; padding: 5px;">DIA</td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">.005</td> <td style="text-align: center; padding: 5px;">TIR A</td> <td></td> </tr> </table>	11.005 B	.125		- B -			.005 TIR A			.005			6.000	DIA		5.500	DIA		.005	TIR A	
11.005 B	.125																					
- B -																						
.005 TIR A																						
.005																						
6.000	DIA																					
5.500	DIA																					
.005	TIR A																					

NOTES:

1. MADE FOR PF-700-362-04

UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES. TOLERANCES- BREAK EDGES. .005. FRACT. $\pm .004$ INT COR. .005 R MAX DEC. $\pm .005$ ANGLES $\pm 10^\circ$ ALL SURFS. ✓	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 20%;">R5</td> <td style="width: 60%;">ADD GEOM. TOL.</td> <td style="width: 20%; text-align: right;">2-2-63 H.W.</td> </tr> <tr> <td>R4</td> <td>CHG. TITLE</td> <td style="text-align: right;">2-2-70 E.E.</td> </tr> <tr> <td>R3</td> <td>CHG. TITLE</td> <td style="text-align: right;">6-18-70 H.G.</td> </tr> <tr> <td>R2</td> <td>CHANGED TITLE</td> <td style="text-align: right;">5-6-65 H.G.</td> </tr> <tr> <td>R1</td> <td>TITLE WAS: RING, SLIP</td> <td style="text-align: right;">11-14-63 H.G.</td> </tr> </table>	R5	ADD GEOM. TOL.	2-2-63 H.W.	R4	CHG. TITLE	2-2-70 E.E.	R3	CHG. TITLE	6-18-70 H.G.	R2	CHANGED TITLE	5-6-65 H.G.	R1	TITLE WAS: RING, SLIP	11-14-63 H.G.
R5	ADD GEOM. TOL.	2-2-63 H.W.														
R4	CHG. TITLE	2-2-70 E.E.														
R3	CHG. TITLE	6-18-70 H.G.														
R2	CHANGED TITLE	5-6-65 H.G.														
R1	TITLE WAS: RING, SLIP	11-14-63 H.G.														

STANFORD LINEAR ACCELERATOR-M U.S. ATOMIC ENERGY COMMISSION MAT'L. CERAMIC - AL-360	TITLE RING, BACK UP VK-5 KLYSTRON
ENGR. J.G. GREENHILL CHK'D. H.G. DFTS. GREENHILL 2-6-63 APPV'D	DATE 2-6-63 SCALE 1"=1"
	PF-700-648-01-RE



NOTE

1. TWO DIA'S. A TO BE CONC. WITHIN .005 T.I.R.
 2. TWO SURFACES S TO BE FLAT, PARALLEL TO EACH OTHER & PERPENDICULAR TO & WITHIN .005 T.I.R.
- "

ALL DRAWINGS ARE IN INCHES
UNLESS OTHERWISE SPECIFIED
TOLERANCES: BREAK EDGES. .005-.015
FRACT. $\pm .004$ INT. COR. .015 R. MAX.
DEC. $\pm .005$
ANGLES $\pm 1^\circ$ ALL SURFS.

UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES.
TOLERANCES: BREAK EDGES. .005-.015
FRACT. $\pm .004$ INT. COR. .015 R. MAX.
DEC. $\pm .005$
ANGLES $\pm 1^\circ$ ALL SURFS.

STANFORD LINEAR ACCELERATOR-M
U.S. ATOMIC ENERGY COMMISSION

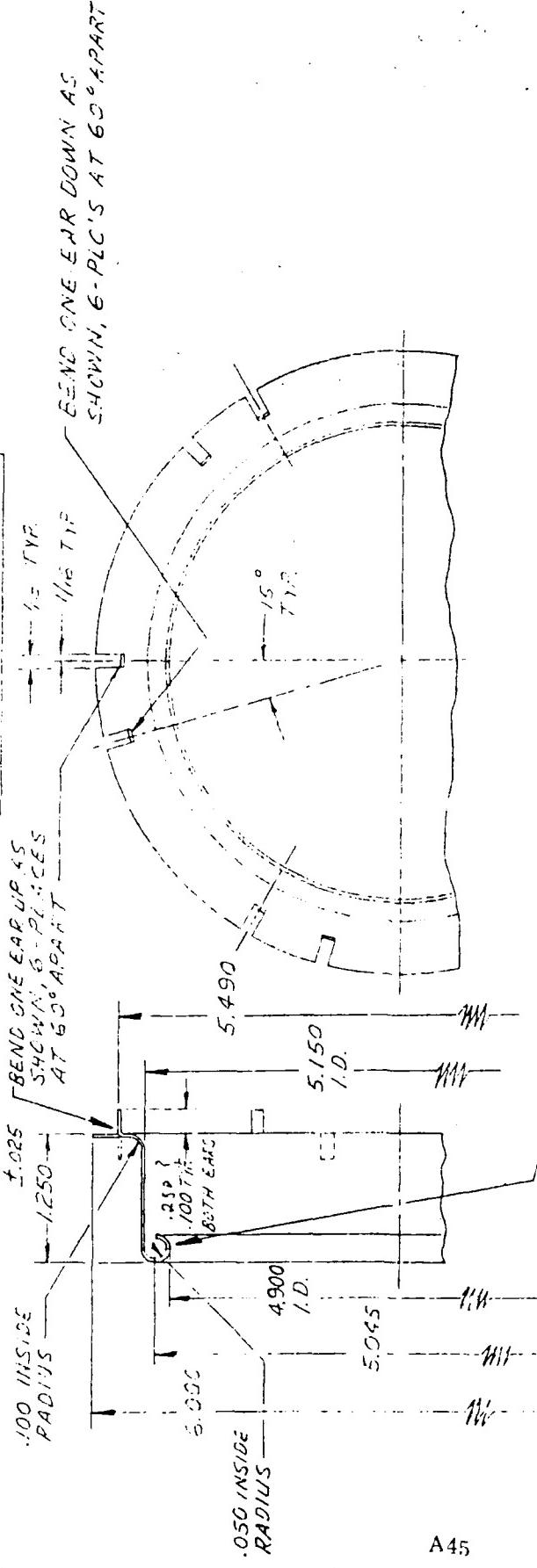
MAT'L. CERAMIC - AL-300

ENGR. MERRILLIAN CHK'D H.G.
DFTS GREENHILL 2-6-63 APPV'D G.P.W.H.

R3	CHG. TITLE	H-23-76	RE- 3-2
R2	CHG. TITLE	B-18-70	R.E.C.
R1	CHANGED TITLE	5-6-65	R.E.B.

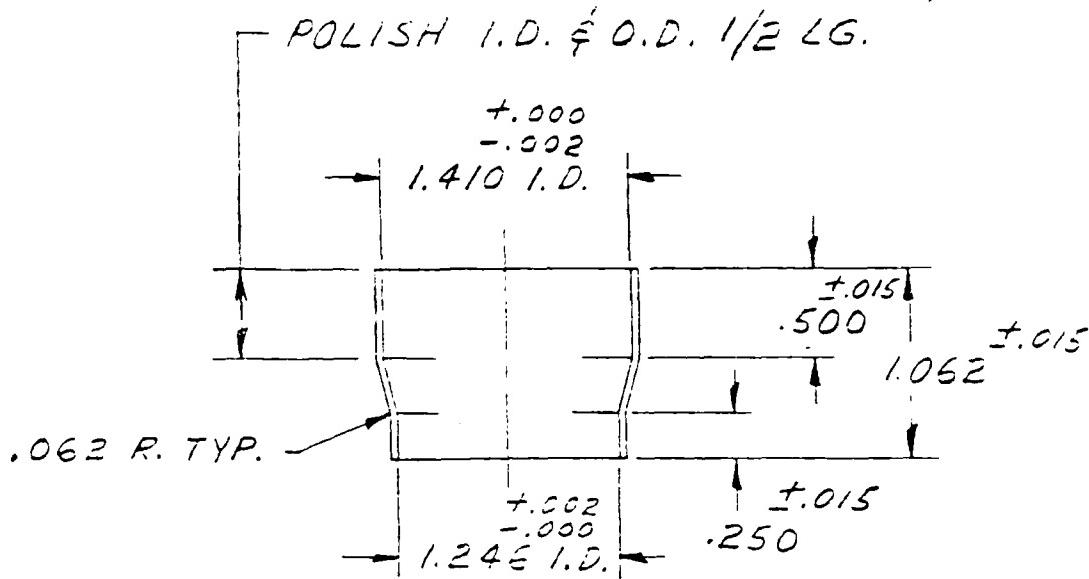
TITLE	CERAMIC XK-5 KLYSTRON
DATE 2-6-63	PF-700-649-01-R3

PF-700-652-01-FE



A45

1. SELECT C-125 THT. ELECT. GRADE A' NICKEL	1.95	RECEIVED	11-11-76 G-2
2. SCAFFOLD SIZE = $\frac{1}{16}$ " SQ. OR $\frac{3}{16}$ " RD.	1.00	FINAL	11-11-76 G-2
3. LINEARIZING AT 700°C. FOR 5-MIN.			
4. CUTTING PC BOARD AND SLITTING EARS, POLISH BEFORE ANNEALING AT 700°C. FOR 10 MIN. (DO NOT BEND FINS OR TUBE AFTER PC BOARD CUTTING)			
STANFORD LINEAR ACCELERATOR - M U.S. ATOMIC ENERGY COMMISSION		ONE P/NG. CORONA A/C	
TEST PERIODICALLY CHECKED ON SCAFFOLD 2-1/2" X 4"	12.5	DATE 11-15-76 SCALE 1/16"	PF-700-650-2-1-5-



NOTE:

1. MAT'L: .020 THK. 70-30 CUPRO-NICKEL
2. BLANK SIZE = 3.010 DIA
3. CHEMICAL CLEAN
4. ANNEAL AT 800 - 850°C. FOR 20 MIN.
BEFORE DRAWING
5. CHEMICAL CLEAN
6. STRESS RELIEVE AT 800°-850°C. FOR 20 MIN.
BEFORE MACHINING

13 SEP 1978

UNLESS NOTED
TOLERANCES BREAK CORNER .005
FRCT. ± 1/64 INT. RADII .015
DEC. ± .005 63
ANGLES = 1/2"

RS	REV. NOTES	7-16-71 H.G.	13
R4	DEL. NOTES 5 & 6. CHANGED TITLE	1-23-70 H.G.	PC
R3	REVISED NOTES	7-17-69 H.G.	KLC
R7	ADDED POLISH NOTE	9-13-78 H.G.	13
R6	CHANGED TITLE	7-23-71 H.G.	13

STANFORD LINEAR ACCELERATOR-M
U.S. ATOMIC ENERGY COMMISSION

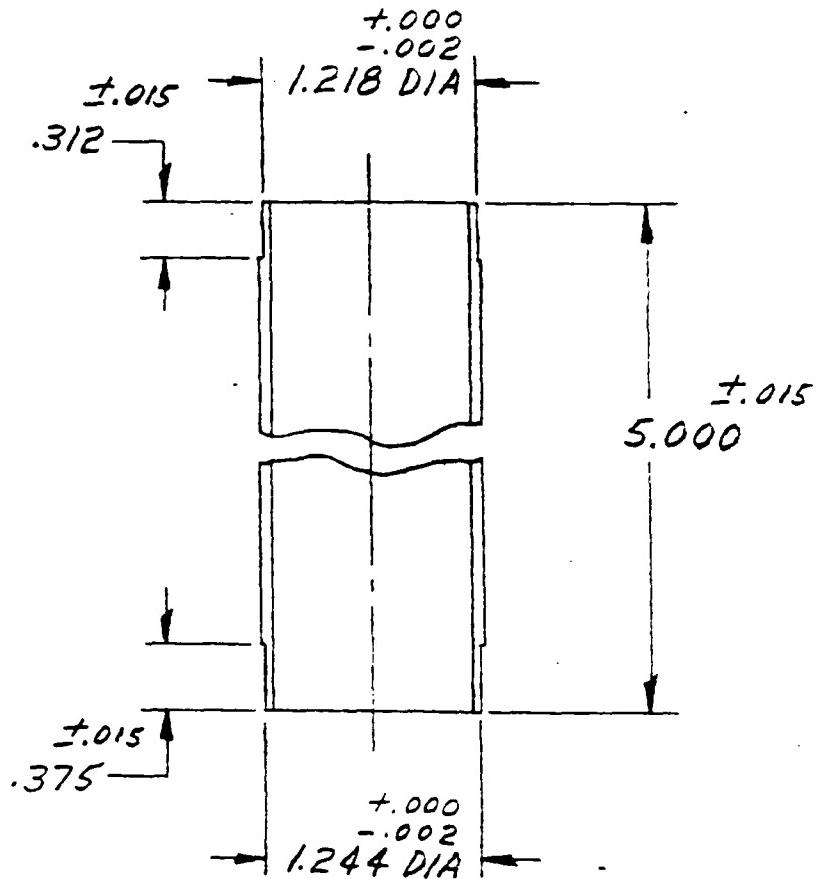
TITLE CUP, SEALING-MALE
XK-5 KLYSTRON

ENGR. MERDINIAN CHK'D H.G.
DFTS. GREENHILL 3-12-63 APPV'D M.C. Com

DATE 3-12-63

SCALE 1"=1"

PF-700-654-01-R7



NOTE:

1. MACHINED SURFACES ³²/
2. POLISH STOCK O.D.

UNLESS NOTED
 TOLERANCES BREAK CORNER .005
 PRACT \pm 1/64 INT. RADIUS .015
 DEC. \pm .005
 ANGLES = 1/2°

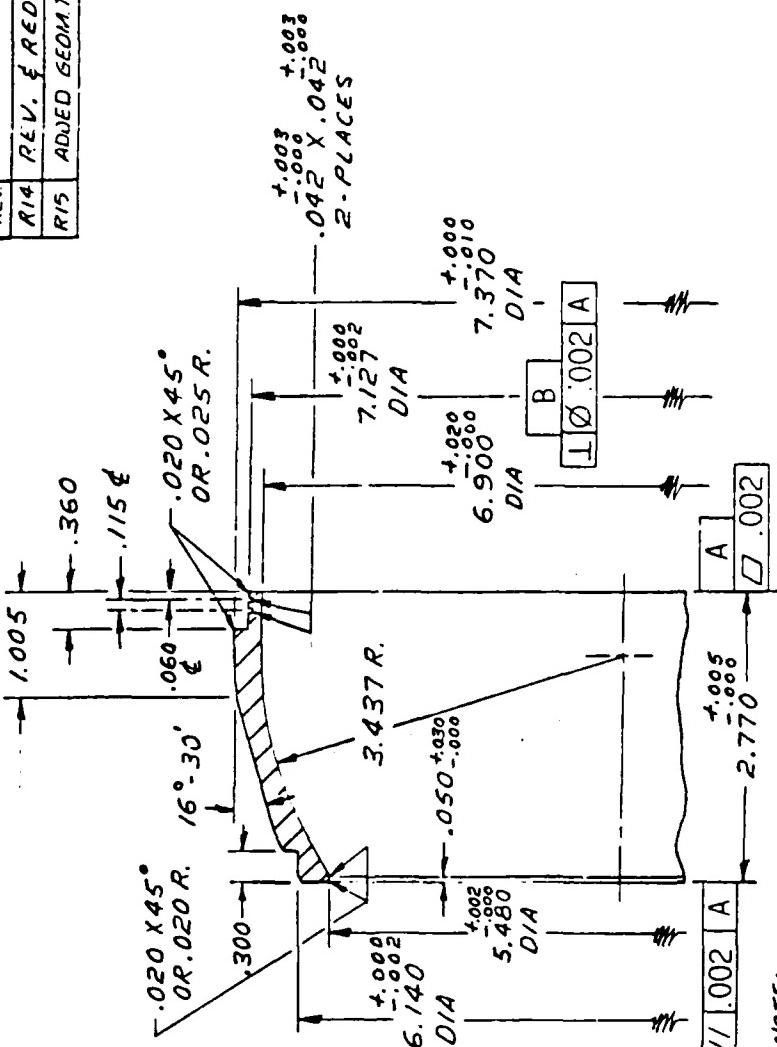
63

S	ADDED NOTE #2.	9-4-50	1975
4	DEL. BRZ. GROOVES	3-21-80	H.G.
R3	CHG. TITLE	11-23-76	A.F.C.
R2	CHG. TITLE	8-18-70	A.R.
R1	CHANGED TITLE	5-6-65	R.E.B.

STANFORD LINEAR ACCELERATOR-M U.S. ATOMIC ENERGY COMMISSION		TITLE TUBE, PUMPOUT XK-5 KLYSTRON	
MAT'L. 1 1/4 O.D. X 1/16 W. CERT. O.F.H.C. CU		DATE 3-12-63	
ENGR. MEKOINIAN	CHK'D H.G.	SCALE 1"=1"	PF-700-655-01-R5
DFTS GREENHILL	3-8-63 APPROV'D Melano		

PF-700-682-01-R15 B

REV.	DESCRIPTION	DRN.	DATE APP	DATE
R14	REV. & REDRAWN	K.G.	4-6-82	WC
R15	ADDED GEOM. TOLER - REV NITE 3	J.G.	7-16-82	RTD 7-16-82

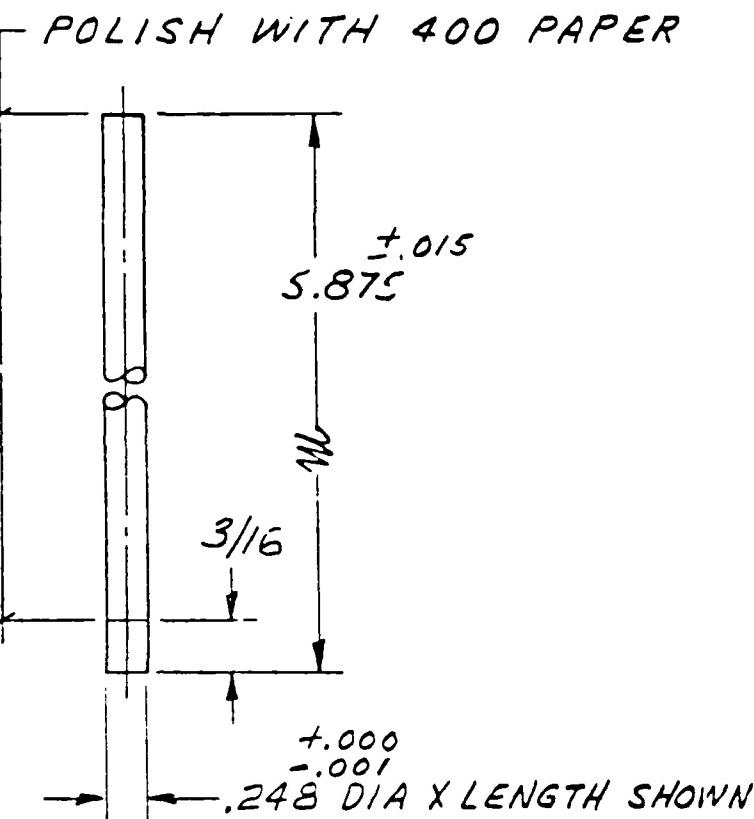


NOTE:

1. MADE FROM PF-700-301-03
 2. STRESS RELIEVE AT 550-1000 °C.
 3. USE ONLY SLAC APPROVED MACHINING FLUID PER SC-700-EGG-97

ITEM NO	PREFIX	BASE	SUFFIX	TITLE OR DESCRIPTION	QTY
	STOCK	OR PART NO			
SCALE	"/"		DO NOT SCALE DRAWING	NEXT ASSEMBLY SA-700-77C-01	
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ARE ± .005 UNLESS NOTED FRAC T : INT COR 315 A MAX DEC : .005 ALL Holes : ANVILS :	STANFORD LINEAR ACCELERATOR CENTER NS INSTITUTE OF PHYSICS STANFORD UNIVERSITY STANFORD CALIFORNIA APPROVED R. E. STENBERG R. GREENWELL PFC			HOUSING, ANODE XK-5 KLYSTRON PF-700-682-01-F:51 B	

四



NOTE:

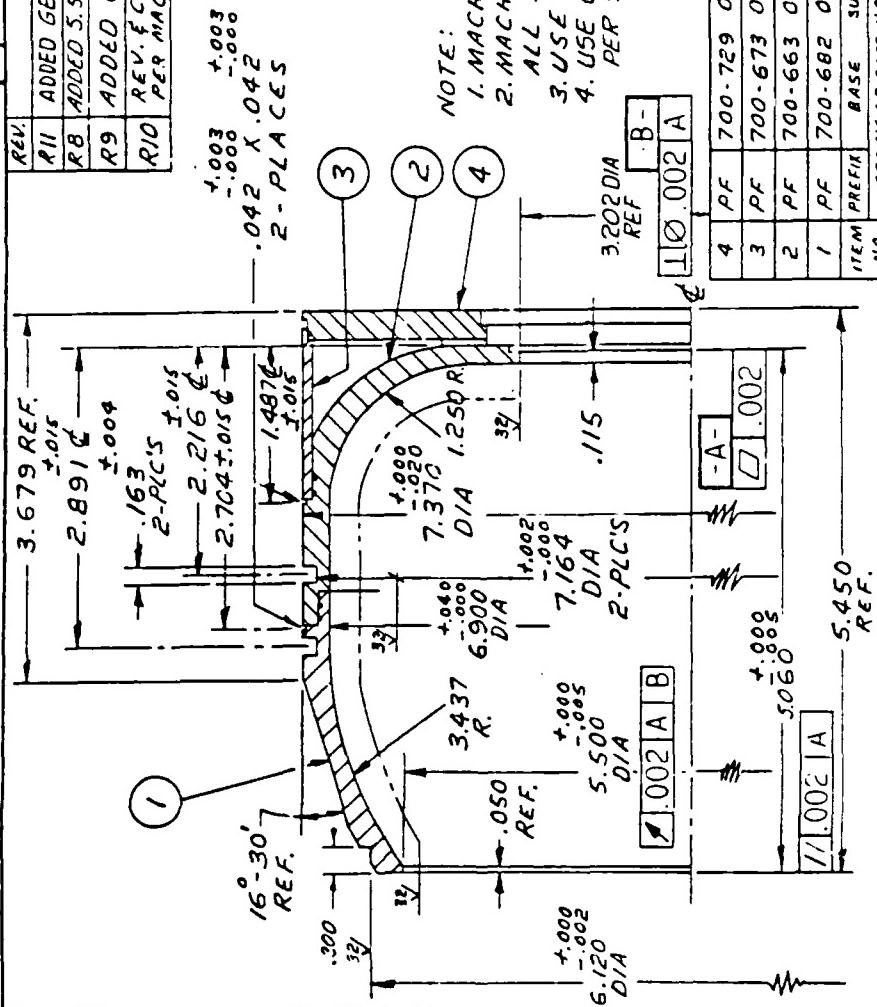
1. MAT'L: 1/4 DIA 304 L STN STL ROD
2. USE ONLY SLAC APPROVED MACHINING FLUIDS PER SC-700-866-47
3. NEXT ASSY: SA-700-783-01

R6	3/16 WAS 5/16 & 5.875 WAS 6.000	3-81-80 S.S.	3-81-80 H.G.
R5	ADDED POLISH NOTE	2-1-80 H.G.	H.I.C.
R4	CHG. TITLE	11-15-76 B.E.	L-TK
R3	ADDED .248 DIA X 5/16 LG.	5-28-71 H.G.	I.R.
R2	CHG. TITLE	6-18-70 H.G.	I.N.C.
R7	ADDED NOTES 2 & 3	12-14-73 H.G.	2-3-74 D-16
STANFORD LINEAR ACCELERATOR U.S. ATOMIC ENERGY COMMISSION	TITLE	ROD. CENTER HEATER XK-5 KLYSTRON	
ENGR G. MENGELIA, JR. CHKD. F.M.	DATE	2-22-66	
DEPTS H. GREENHILL E.D.O. APPV'D	SCALE	1" = 1"	
		PF-700-759-01-R7	

M.F.: 7

SA-700-770-01-R1/B

REV.	DESCRIPTION	DRAWN BY	APR DATE
R11	ADDED GEOM TOLER- NOTE 4	J.G.	12-10-81
R8	ADDED 5.500 DIA F. 300±5.000 DEF.	J.G.	12-10-81
R9	ADDED 6.120 DIA	J.G.	12-10-81
R10	REV. & CHANGED SEVERAL DIM'S DOD AND CIRCLES	H.G.	6-9-82



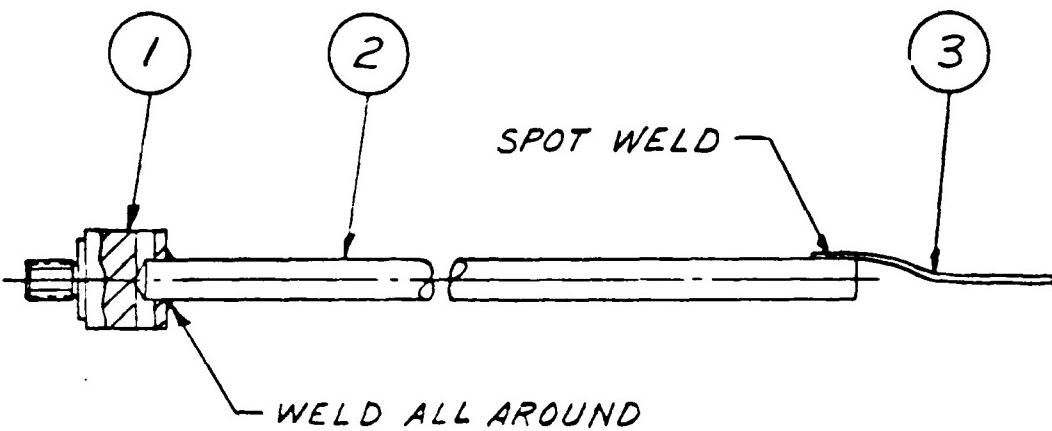
NEUT ASSEMBLY: SA-700-857-02
 ASSY, ANODE SHELL (MACH)
 XK-S ALYSTRON
 SA-700-770-01-R11 B

SCALE: 1" = 1'-0" NO. 5000 OR PART NO.

ASSY, ANODE SHELL (MACH)
XK-5 KLYSTRON
SA-700-770-01-RII B

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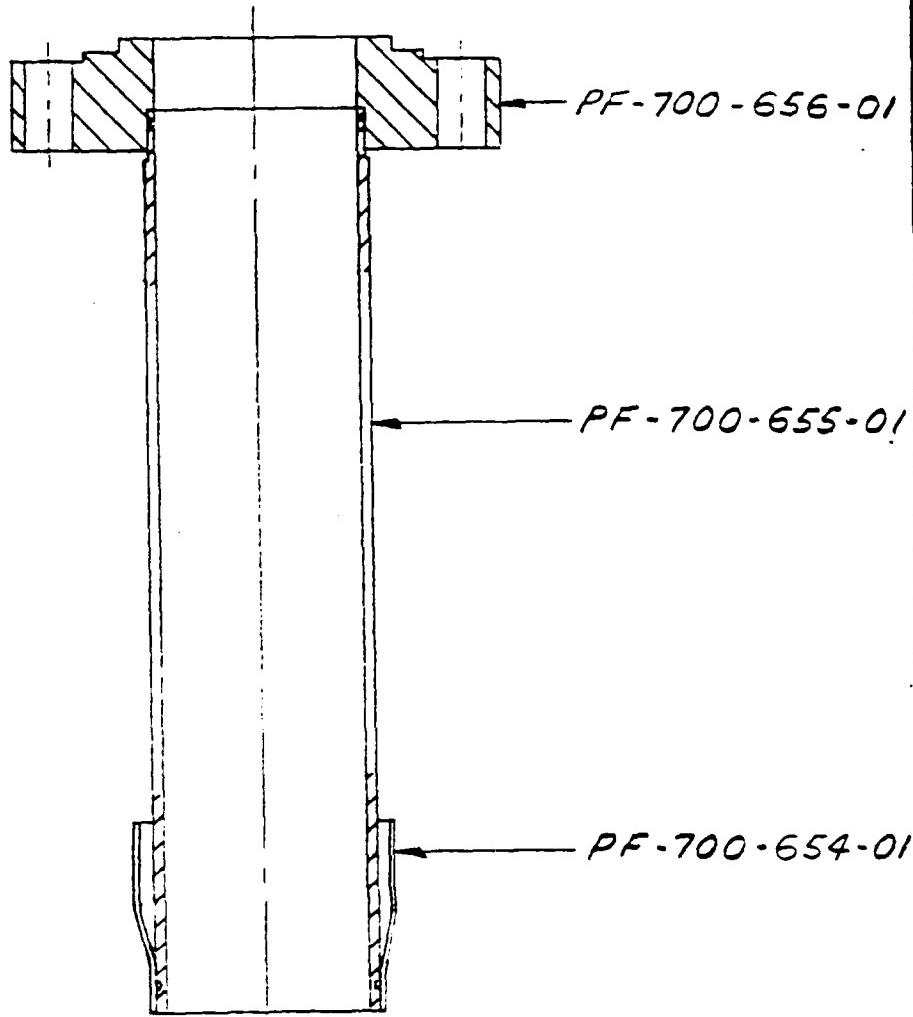
NOTE:

1. NEXT ASSY: SA-700-786-01

ITEM NO.	PREFIX	BASE	SUFF.	DESCRIPTION	QTY.
3				.005 THK. X. 300X1.5 LG. NICKEL STRIP	4
2	PF	700-759	01	ROD, CENTER HEATER	1
1	PF	700-229	01	CYLINDER	1

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R1	CHG. TITLE	H.G.	8-18-70	FAC	8-5-70
R2	CHG. TITLE	B.E.	11-5-70	LTK	11-15-70
R3	.300 WAS .287	S.S.	5-2-71	H.G.	6-11-70
R4	ADDED NOTE 1.	H.G.	12/14/83	RTB	2/2/94

STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		ASM. CTR. HEATER COND. XK-5 KLYSTRON		
ENG'D. P.C. MILLER DPTS. H.G. SEINHILL CHE F. J. L.	APPROVALS 1-3-69	SA-700-783-01-R4	A	PAIK

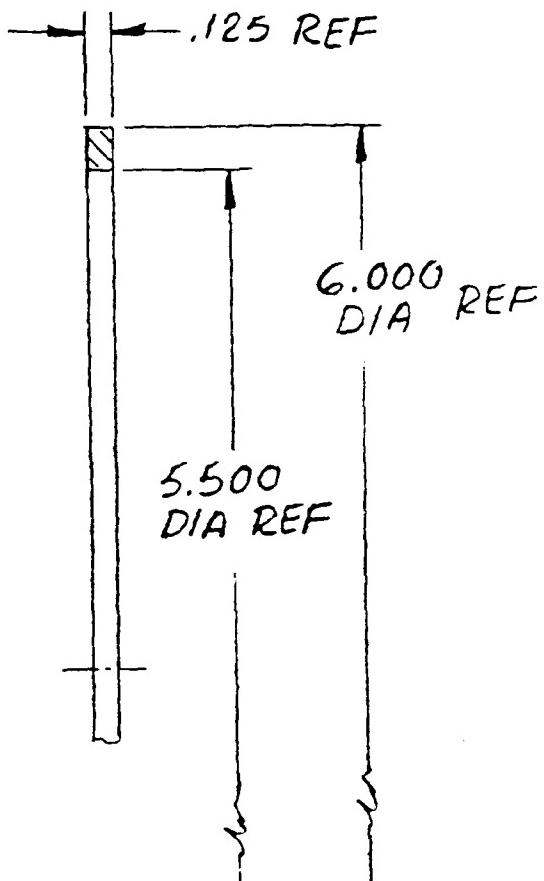


SCALE: 1" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE

14 JUL 1973

STANFORD LINEAR ACCELERATOR CENTER U.S. ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION STANFORD UNIVERSITY STANFORD CALIFORNIA		APPROVALS	ASSY, PUMPOUT XK-5 KLYSTRON		
ENG'D DRAFTS C.H.E.	G. RONRAD H. GREENHILL CPA 7-17-78	1427	SA-700-857-17-RO	A	



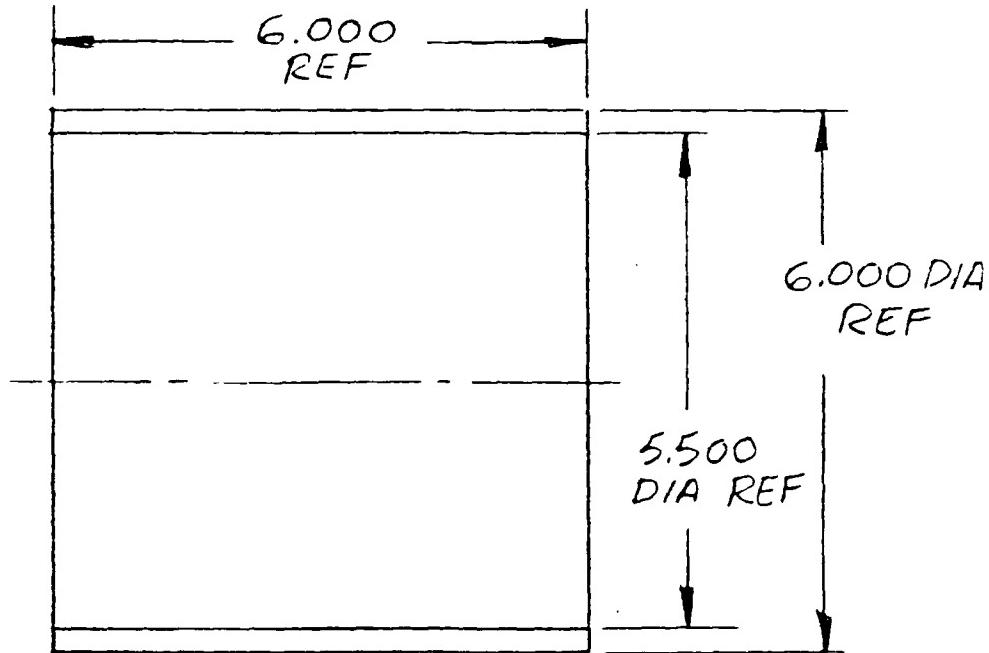
NOTE:

1. MADE FROM PF-700-648-01
2. OFHC Cu. PLATE 0.0002 ALL METALLIZED SURFACES.

SCALE: 1" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE

STANFORD LINEAR ACCELERATOR CENTER U.S. DEPARTMENT OF ENERGY STANFORD UNIVERSITY STANFORD, CALIFORNIA		RING, PL - BACK UP XK-5 KLYSTRON	
ENGR R. BOESENBERG DFTS M. WALLACE CHK H.G.	APPROVALS 2-24-82	PF-700-862-04-RO	A



NOTE:

1. MADE FROM PF-700-649-01
2. OFHC Cu. PLATE 0.0002 ALL METALLIZED SURFACES

SCALE: $\frac{1}{2}'' = 1''$

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE

STANFORD LINEAR ACCELERATOR CENTER U.S. DEPARTMENT OF ENERGY STANFORD UNIVERSITY STANFORD, CALIFORNIA	CERAMIC, PLATED XK-5 KLYSTRON
ENGR. R. BOESENBERG DFTS M. WALLACE CHK H. G.	APPROVALS 2-24-82 PF-700-862-05-R0 A

APPENDIX A-4
PARTS AND MATERIALS LIST

10 FIN-RA001 ALABAMA
REQUEST UNIT CODE 01 PART NUMBER 00-192143-00 REV C DESCRIPTION NRL GUN ASSY K9025 CTY 1

ENGINEERING INDENTED EXPLOSION

FEB 6, 1986 MDAY 793 PAGE 1

LOW LEVEL	UC 2	PART NUMBER	DW OS	RV RV	DESCRIPTION	UI	QUANTITY PFR ASSY	QUANTITY M CTR	ITEM DATA				CUM LT	RIF M
									TOTAL	E WK	ENGRN FFDT/SRL	OPN		
1	A	27-402483-00	TT	O RING CRANE 1820-67 EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192192-00	*	ANODE & CONFLAT ASSY EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192193-00	*	ANODE ASSY MACH	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	D	00-192194-00	*	ANODE	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-192195-00	*	CONFLAT ADPTR SLEEVE	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192196-00	*	ANODE JACKET	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192197-00	*	COLDIANT FITTING	EA	2.0000	2.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192198-00	*	HOUIS SEAL RING ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192199-00	*	ANODE HOUSING ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192201-00	*	WELD RING A	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192200-00	*	IRON HOUSING ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192202-00	*	WELD RING B	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192203-00	*	WELD RING C	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	D	00-192204-00	*	IRON HOUSING	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192207-00	*	GUN COIL	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192206-00	*	BOBBIN	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	12-312006-08	TT	6-32 X 1/2 SCHCSCR	EA	6.0000	6.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	81-101918-00	TT	1BAWG MAGNET WIRE	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	81-249882-00	TT	WIRE 16ANGREDTEFLONI	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	81-249986-00	TT	WIRE 16ANGBLUETEFLONI	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192222-00	*	CATH STEM SUPP ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192209-00	*	INNER HEAT SHLD ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192210-00	*	HEATER CATH PKG ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	07-664006-00	TT	.005X .100 PURE PLAT	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	C-166501-00	E	D LEAD SUPPORT ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-142138-00	*	LEAD BUSHING STOP	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	Q2-451500-60	TT	.062 DIA .01A RD NICKEL B	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	07-166001-50	TT	.015 DIA .35/65 AUCU	EA	5.0000	5.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-051834-00	*	* LEAD SUPPORT	EA	2.0000	2.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-166486-00	C	* MTLZD BUSHING	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-166487-00	C	* LEAD BUSHING	FA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-166789-00	C	A BRAZING WAFER	EA	2.0000	2.000 0	000000	000000	000000	000000	000000	000 1.00	
1	A	00-166790-00	*	A LEAD WASHER	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	C	00-192181-00	*	CATHODE STEM ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192182-00	*	STEM SUPPORT A	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192183-00	*	STEM SUPPORT B	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192184-00	*	STEM SUPPORT C	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192185-00	*	FOCUS ELECTRODE ASSY	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192186-00	*	FOCUS ELECTRODE SLEEVE	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192187-00	*	CATH SUPPORT SLEEVE	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	
1	B	00-192189-00	*	FOCUS ELECTRODE	EA	1.0000	1.000 0	000000	000000	000000	000000	000000	000 1.00	



APPENDIX E

"ELECTRON GUN BREAKDOWN"

by

Dr. Armand Stavans, Varian Associates, Inc.

1985 High-Voltage Workshop

February 26, 1985

Monterey, California



ELECTRON GUN BREAKDOWN

ARMAND STAPRANS

VARIAN ASSOCIATES, INC.

PRESENTED AT THE
1985 HIGH-VOLTAGE WORKSHOP
FEBRUARY 26, 1985
MONTEREY, CALIFORNIA

Electron Gun Breakdown

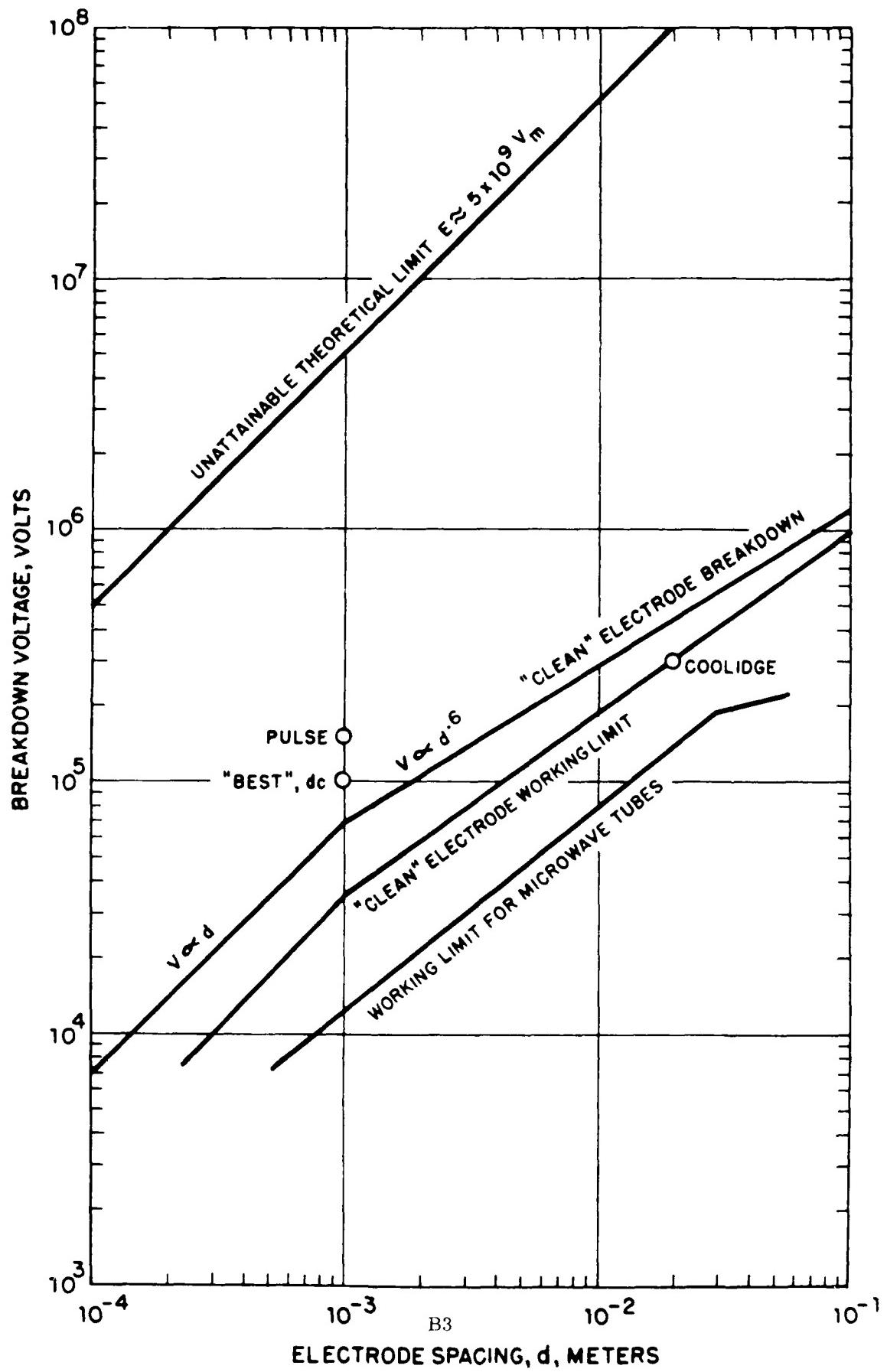
A. Staprans
Varian Associates Inc.
611 Hansen Way
Palo Alto, CA 94303

The electron gun is usually the portion of a microwave tube that is most stressed by high voltage and is frequently subject to breakdown. This is a consequence of design constraints which often require the use of close-spaced vacuum gaps between gun electrodes.

The design criteria for voltage hold-off in guns are reviewed. Largely because of the presence of evaporation from a hot cathode, the acceptable safe voltage between gun electrodes is substantially lower than for a similarly spaced "clean" vacuum gap. Design guidelines for achieving adequate voltage hold-off in guns are discussed, including allowable gradients, electrode spacings, pulse vs dc operation, electrode materials, and insulator configurations.

The tube-power supply interface plays a very important role in minimizing gun breakdown. Arc energy limiting means such as crow-bars and arc current limiting impedances are discussed and design criteria suggested.

VACUUM GAP VOLTAGE BREAKDOWN COMPARISON





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SPECIAL FACTORS IN ELECTRON GUN BREAKDOWN

- PRESENCE OF A HOT CATHODE — BARIUM DEPOSITION ON ELECTRODES
- “LOW” IMPEDANCE POWER SUPPLIES — LARGE AVAILABLE ARC ENERGY
- ELEVATED ELECTRODE TEMPERATURES — ENHANCED FIELD EMISSION
- LARGE ELECTRODE AREA (COMPARED TO SPACING)
- COMPLEX ELECTRODE SHAPES — DIFFERENT FROM SIMPLE GAP THEORIES
- PRESENCE OF MAGNETIC FIELD — AFFECTS CHARGED PARTICLE PATHS
- LIMITED CHOICE OF MATERIALS



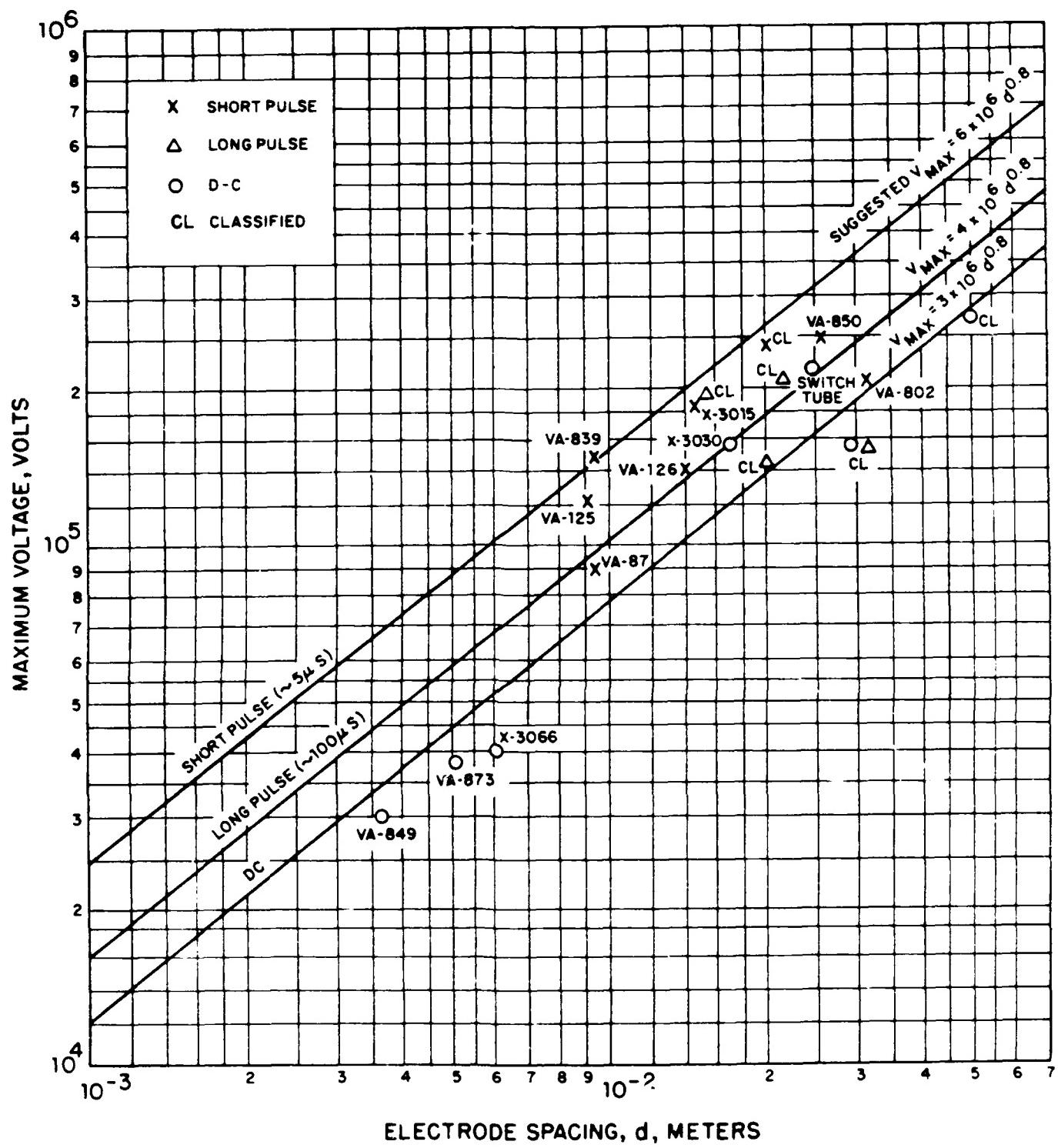
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ELECTRODE SPACING RATHER THAN GAP FIELD IS PREFERRED VARIABLE

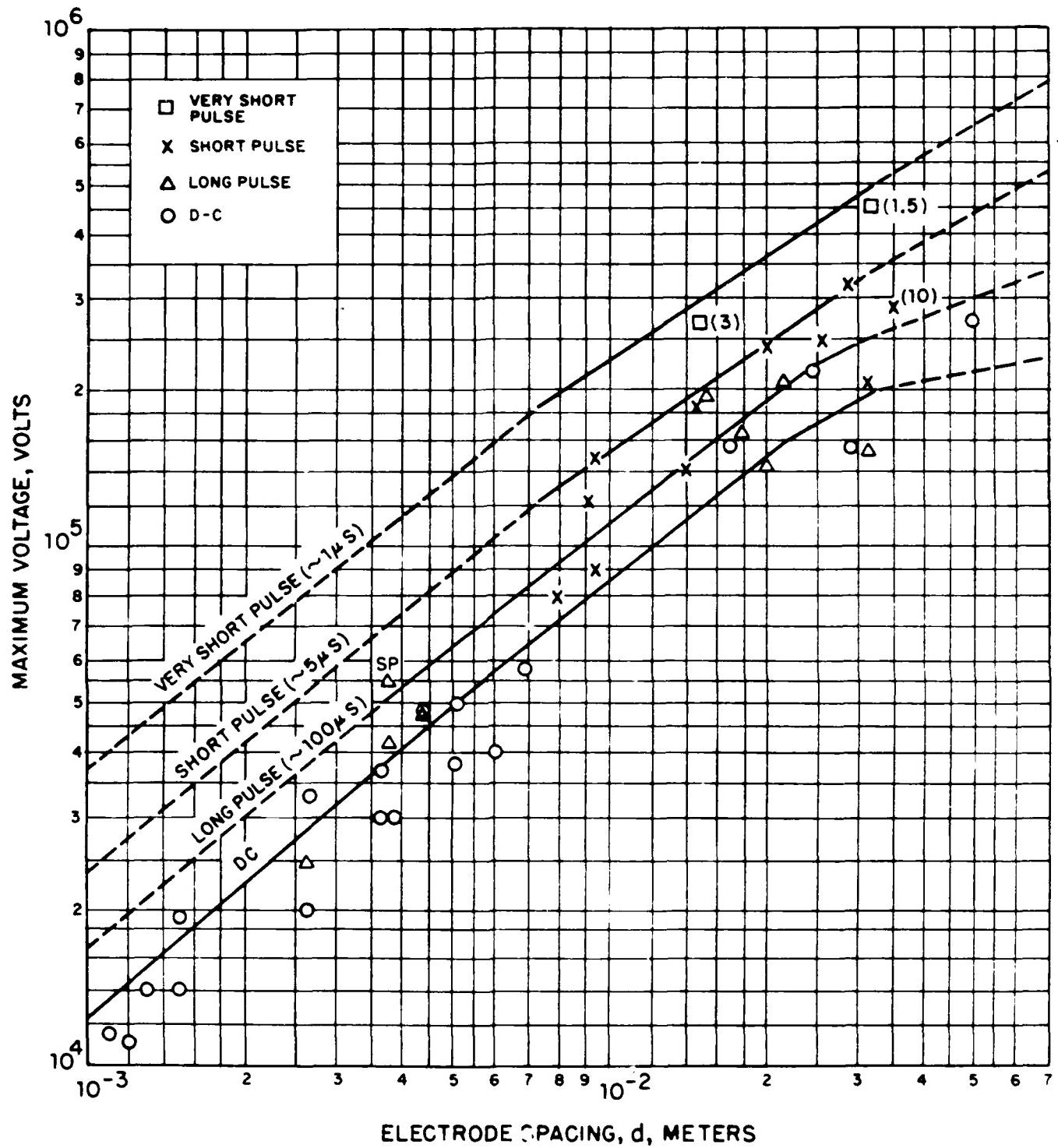
- FIELD AT ELECTRODE SURFACE IS BUT ONE OF MANY FACTORS AFFECTING BREAKDOWN. ELECTRODE SHAPES AND SIZES ARE ALSO IMPORTANT. MINIMUM SPACING IS A GENERAL PARAMETER.
- FOR WELL DESIGNED GUN FOCUS ELECTRODES, FIELD ENHANCEMENT FACTOR ABOVE V/d IS LOW:

USUAL RANGE	1.3 to 1.7
AVERAGE	1.5
- ELECTRODE SPACING DATA IS MORE AVAILABLE THAN GRADIENTS
- EXISTING DATA YIELDS FAIRLY CONSISTENT RESULTS
- CONVENIENT DESIGN PARAMETER

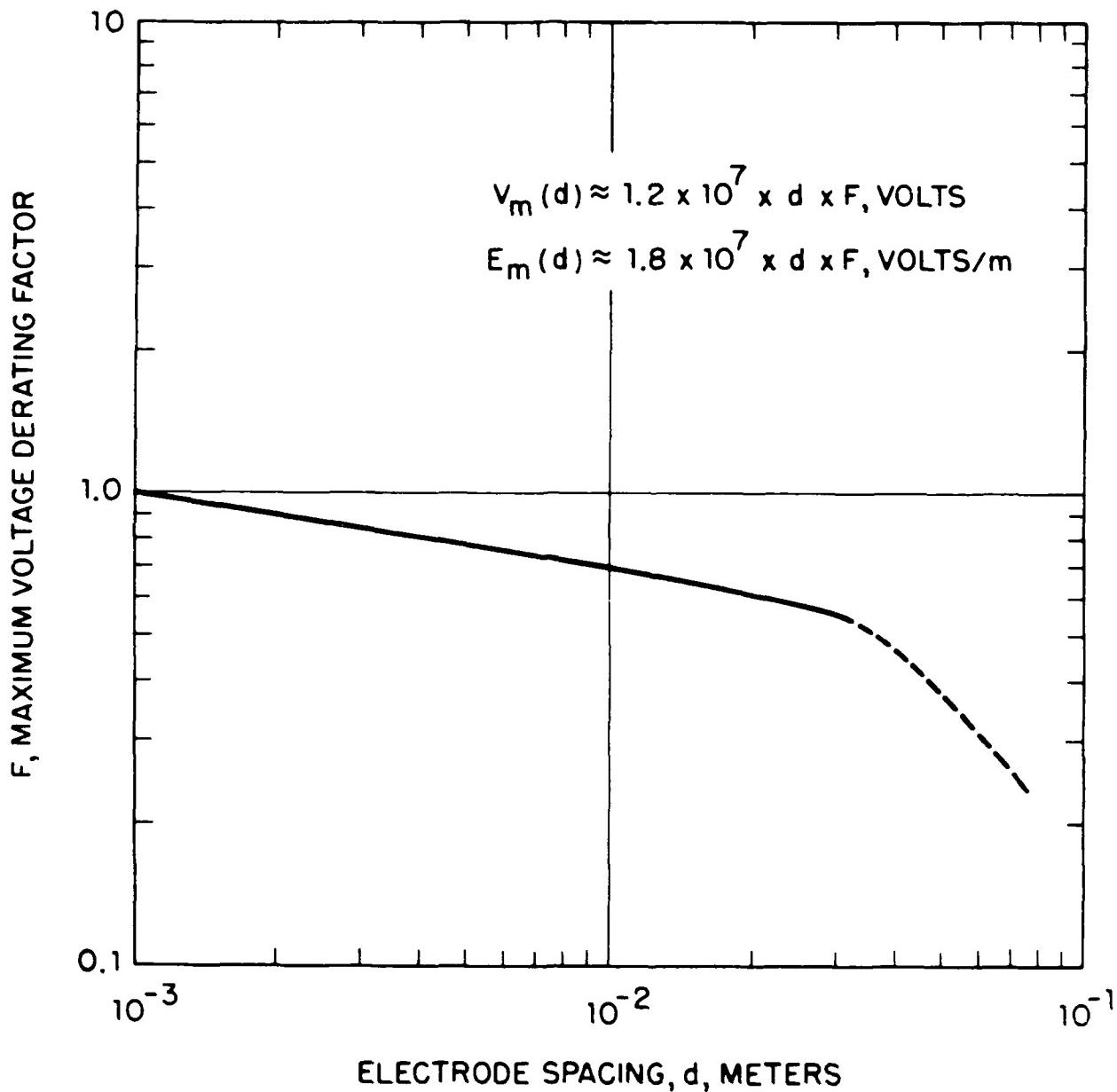
GUIDE TO HV SPACING DESIGN IN ELECTRON GUNS (1966)



GUIDE TO HV SPACING DESIGN IN ELECTRON GUNS (1985)

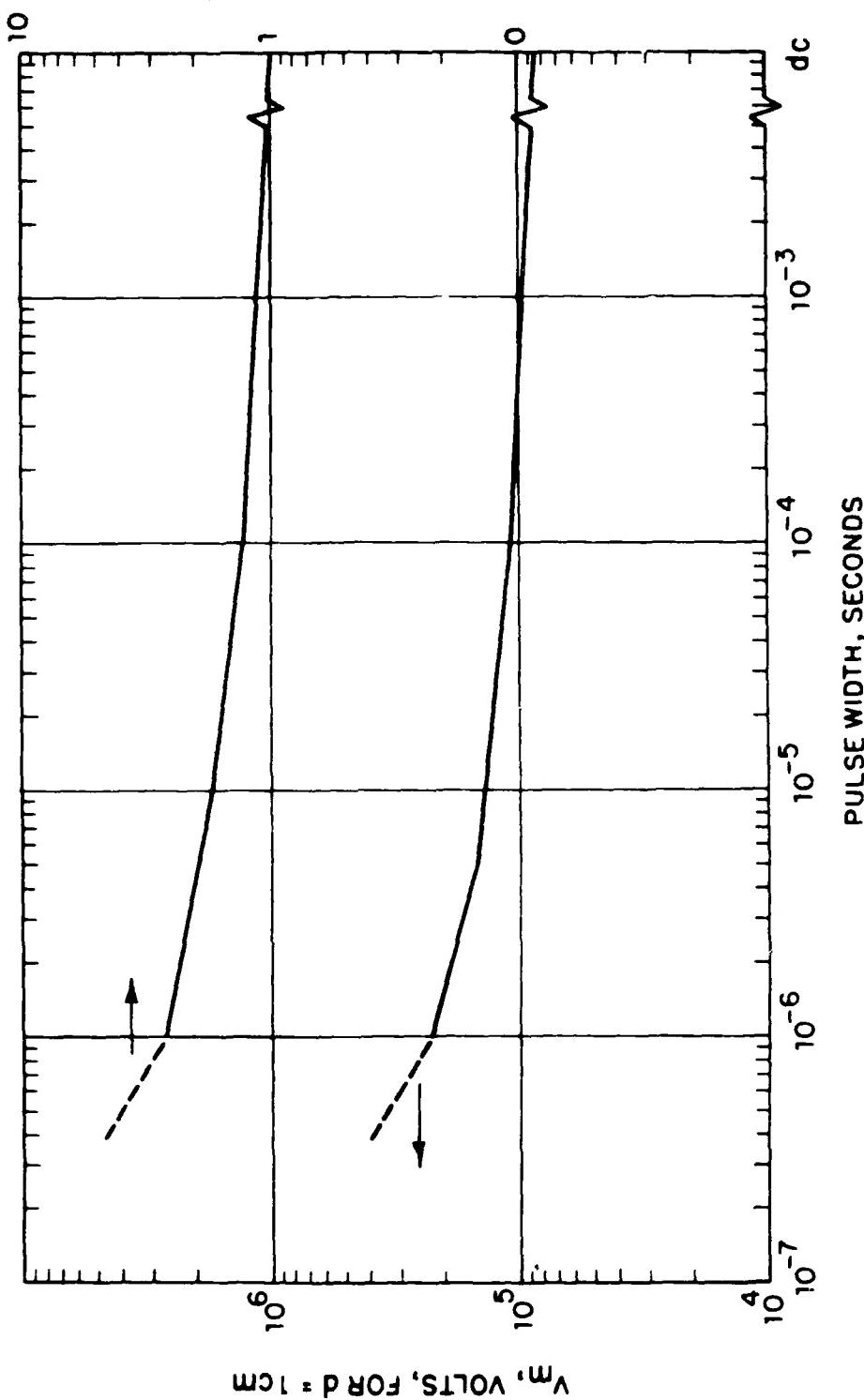


MAXIMUM DESIGN VOLTAGE, V_m , OR FIELD, E_m ,
DERATING FACTOR, F, FOR ELECTRODE SPACINGS
ABOVE 1 mm FOR d.c. CONDITIONS



MAXIMUM DESIGN VOLTAGE, V_m , vs. PULSE WIDTH

VOLTAGE (OR FIELD) ENHANCEMENT FACTOR
FOR PULSES COMPARED TO d.c.





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SUMMARY OF DESIGN CRITERIA

- CURVES OF MAXIMUM VOLTAGE vs ELECTRODE SPACING FOR PULSE AND DC
- ALTERNATELY, FOR MORE APPROXIMATE ESTIMATES AND PARAMETRIC CALCULATIONS, FOR GAPS UP TO ABOUT 3 cm, THE FOLLOWING APPLIES:
$$V_{max} \approx K \times 10^6 d^{0.8}$$
, where
 - K ≈ 3 FOR DC
 - ≈ 4 FOR 100 msec PULSES
 - ≈ 6 FOR 5 msec PULSES
 - ≈ 9 FOR 1 msec PULSES



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ELECTRODE MATERIALS AND SURFACES

- FOR NEGATIVE (FOCUS) ELECTRODE, STAINLESS STEEL (SOMETIMES OXIDIZED) IS COMMON USAGE. IRON AND MOLYBDENUM ARE ALTERNATES. COPPER IS STILL USED FOR THE LOWER VOLTAGES.
- COPPER, STAINLESS STEEL AND IRON ARE USUAL ANODE MATERIALS, BUT STAINLESS STEEL IS PREFERABLE.
- MECHANICAL POLISHING AND SUBSEQUENT CLEANING IS PREFERRED, BUT CARE MUST BE TAKEN TO PREVENT SURFACE CONTAMINATION.
- MICROSCOPIC PROPERTIES OF SURFACES ARE IMPORTANT.



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GUN INSULATOR ISSUES

- SURFACE BREAKDOWN CAN OCCUR FROM ELECTRON EMISSION
FROM THE TRIPLE JUNCTION AND SECONDARY ELECTRON
MULTIPLICATION AND CHARGING, OR FROM SURFACE
CONTAMINATION/LEAKAGE.
- DESIGN CRITERIA FOR CERAMIC INSULATORS:
LENGTH $\sim 10 \times$ THAT OF EQUIVALENT VACUUM GAP
WALL THICKNESS TO WITHSTAND FULL APPLIED VOLTAGE
GROOVED OR ROUGHENED VACUUM SIDE SURFACES
SHIELDING FROM CATHODE, ARC, AND BEAM HEATING
EVAPORANTS
CORONA SHIELDS FOR TRIPLE JUNCTIONS
FIELD CONCENTRATION, IF ANY, ON NEGATIVE END OF
INSULATOR



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ARC CHARACTERISTICS AND PROTECTION CRITERIA

- BUILDUP TIME IS SHORT — TEN(S) OF NANoseconds
- SUBSEQUENT METAL VAPOR ARC DROP IS LOW — ABOUT 20 VOLTS
- ELECTRODE AND LEAD/BUSWORK STORED ENERGY IS ALWAYS AVAILABLE TO THE ARC (BUILDUP) — USUALLY LESS THAN 1 JOULE
- SUBSEQUENT ARC DISSIPATION SHOULD BE LIMITED TO A COMPARABLE VALUE, ~ 1 JOULE, BY PROTECTIVE CIRCUITRY
- COMMON TUBE SPECIFICATION REQUIREMENTS OF LARGER ARC ENERGIES, E.G. 40 JOULES, ARE UNREALISTIC AND ONLY FUNCTION BECAUSE ONLY A SMALL FRACTION OF THIS ENERGY IS DISSIPATED IN THE ARC



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RECOMMENDED MEASURES FOR ~ 1 JOULE DISSIPATION

- KEEP ELECTRODE AND LEAD/BUSWORK CAPACITANCES LOW
- IF POSSIBLE, "ISOLATE" POWER SUPPLY FROM GUN BY PROVIDING A TIME CONSTANT MUCH LARGER THAN ARC BUILDUP TIME
- FOR UP TO ABOUT 20 KV, A 50 TO 100 Ω SERIES RESISTOR, AND ARC CURRENT LIMITATION TO ABOUT 100 A IS ADEQUATE
- FOR VOLTAGES ABOVE ABOUT 40 KV, AN ELECTRONIC CROWBAR IS USUALLY NECESSARY, ITS SPEED DEPENDENT UPON CURRENT. LIMITING CHARACTERISTICS OF THE SUPPLY:
 - 100 A MAX \rightarrow 0.5 msec CROWBAR
 - 10,000 A MAX \rightarrow 5 μ sec CROWBAR



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SUMMARY

- NO SIGNIFICANT IMPROVEMENTS IN GUN VOLTAGE CAPABILITY
IN THE LAST 20 YEARS, BUT:
- SIGNIFICANTLY BETTER UNDERSTANDING OF VACUUM ARCS EXISTS
- DESIGN LIMITS AND TECHNIQUES ARE BETTER UNDERSTOOD
- PROTECTIVE CIRCUITS ARE BETTER UNDERSTOOD AND ACCEPTED



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ACKNOWLEDGEMENT

MOST OF THE ELECTRON GUN DATA USED WAS OBTAINED FROM:

VARIAN MICROWAVE TUBE DIVISION

VARIAN BEVERLY MICROWAVE DIVISION

STANFORD LINEAR ACCELERATOR CENTER (G. KONRAD)

LITTON ELECTRON DEVICES (R. TRUE)